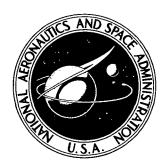
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NASA TM X-3345

PERFORMANCE OF INLET STAGE OF TRANSONIC COMPRESSOR

Donald C. Urasek, Ronald J. Steinke, and George W. Lewis, Jr.

Lewis Research Center

Cleveland, Ohio 44135



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PERFORMANCE OF INLET STAGE OF TRANSONIC COMPRESSOR by Donald C. Urasek, Ronald J. Steinke, and George W. Lewis, Jr. Lewis Research Center

SUMMARY

The first stage of a transonic multistage compressor was tested with inlet guide vanes. Radial surveys of the flow conditions in front of the inlet guide vanes (IGV's), between the IGV's and the rotor, between the rotor and stator, and behind the stator were made over the stable operating flow range of the stage at the design tip speed of 426 meters per second. The surveys were taken at 11 radial positions and all resulting flow and performance calculations were translated to the blade leading and trailing edges. Peak efficiency for both the rotor and stage occurred at 28.8 kilograms per second as compared to the design value of 29.7 kilograms per second. Rotor and stage peak efficiency values were 0.86 and 0.83, respectively, as compared to the design values of 0.88 and 0.86. Corresponding values of total pressure ratio at peak efficiency weight flow for the rotor and stage were 1.56 and 1.52, respectively, as compared to the design values of 1.62 and 1.61. The stall margin for the stage was 8 percent, based on pressure ratio and weight flow at peak efficiency and stall conditions. The stage appears to be stalling prematurely as evidenced by high rotor tip losses, deviation angles, and low velocity ratios. This may, in part, be a result of what appears to be a relatively thick boundary layer entering the rotor resulting in locally high incidence angles. The low velocities leaving the rotor tip results in high incidence angles to the stator in the tip region.

INTRODUCTION

The NASA Lewis Research Center is engaged in a research program on axial-flow compressors for advanced airbreathing engines. The program is directed primarily towards providing the technology to permit reducing the size and weight of the compressor while obtaining higher levels of performance. In support of this program a 51-centimeter-diameter, five-stage compressor having a design weight flow of 29.7 kilograms per second with a pressure ratio of 9.27 was fabricated and tested with inlet

guide vanes (IGV's). Stage matching problems were apparent in the initial testing of this compressor. Limited performance data obtained from these tests indicated that the first stage was not meeting its design performance which may have caused or at least appeared to be contributing to the matching problem. To more completely evaluate the performance of the first stage compressor with its IGV's, it was separately tested in the Lewis single-stage test facility.

This report presents the design data and experimental performance of the first stage of the five-stage compressor with IGV's. The stage, designated stage 66 (inlet guide vanes, rotor 66, stator 66) has a design pressure ratio of 1.61 at a design weight flow of 29.7 kilograms per second. Design efficiency for the stage is 0.863.

The data presented in this report are in tabular as well as in plotted form. The symbols are defined and the equations are given in appendixes A and B. The definitions and units used for the tabular data are presented in appendix C.

AERODYNAMIC DESIGN

Three computer programs were used in the design of the five-stage compressor. These programs are (1) streamline analysis program, (2) blade geometry program, and (3) blade coordinate program. These three computer programs are presented in detail in references 1 and 2, and only a brief description of each is presented in this report.

The streamline analysis program was used to calculate the flow field parameters at several axial locations including planes approximating the blade leading and trailing edges for both the rotor and stator. The weight flow, rotative speed, flow path geometry, and radial distributions of total pressure and temperature are inputs in this program. The program accounts for both streamline curvature and entropy gradients. Boundary layer blockage factors are also included.

The distributions of velocity, total pressure, and total temperature calculated in the streamline analysis program are utilized in the blade geometry program to compute blade geometry parameters. Total loss for the blades was primarily based on the experimental rotor loss data presented in reference 1 with modifications caused by influences of other data which is unreported at this time. The profile loss was then estimated by subtracting a calculated shock loss from the total loss. The shock loss calculation was based on the method presented in reference 3.

The blade geometry parameters are utilized in the blade coordinate program (ref. 2) to compute blade elements on conical surfaces passing through the blade row. In this program the blade elements are then stacked on a line passing through their centers of gravity and cartesian blade coordinates are computed which are used directly in fabrication.

The overall design parameters for the rotor and stator are listed in table I and the flow path is shown in figure 1. This stage was designed for an overall pressure ratio of 1.61 at a weight flow of 29.7 kilograms per second (196 (kg/sec)/m² of annulus area). Design stage efficiency (rotor inlet to stator outlet) is 0.863.

The design tip speed was 426 meters per second. The rotor and stator were designed for tip solidities of 1.4 and 1.5, respectively. The rotor had 57 blades with an aspect ratio of 3.1 and the stator had 64 blades with an aspect ratio of 2.7.

The blade-element design parameters for the rotor are presented in table II. This rotor was designed for a radially constant total pressure ratio of 1.62. The stator blade-element design parameters are given in table III. The blade geometry is presented in table IV for the rotor and in table V for the stator. The rotor has multiple circular-arc blade shapes while the stator had a double circular-arc blade shape.

The equations used for calculating overall blade-element performance parameters are presented in appendix B. All definitions and units presented in the tables are given in appendix C.

A drawing of the inlet guide vane is shown in figure 2. The vanes utilized multiple circular-arc blade profiles. There were 26 vanes having a tip solidity of 1.0 and an aspect ratio of 2.4. Maximum thickness location was at approximately 37 percent of chord from the leading edge. The vanes were made in two segments that could be pivoted at the maximum thickness location. The forward section was stationary while the rear segment was adjustable for varying rotor inlet prewhirl. All tests in this report were conducted with the vanes alined in the axial direction.

APPARATUS AND PROCEDURE

Compressor Test Facility

The compressor stage was tested in the Lewis single-stage compressor facility which is described in detail in reference 4. A schematic diagram of the facility is shown in figure 3.

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Atmospheric air enters the test facility through an inlet located on the roof of the building, flows through the flow measuring orifice and into the plenum chamber upstream of the test stage. The air then passes through the experimental compressor stage into the collector and is exhausted to the atmosphere. Weight flow is controlled with a sleeve valve in the collector.

Test Stage

Photographs of the IGV, rotor, and stator are shown in figure 4. The rotor blades have vibration dampers located at about 40 percent span from the outlet rotor tip. The maximum thickness of the damper is 0.180 centimeter. The nonrotating radial tip clearance of the rotor was a nominal 0.05 centimeter at ambient conditions. To accommodate survey instrumentation, the axial spacing between the IGV hub trailing edge and rotor hub leading edge was 2.50 centimeters. The axial spacing between the rotor hub trailing edge and the stator hub leading edge was 2.66 centimeters.

Instrumentation

The compressor weight flow was determined from measurements on a calibrated thin-plate orifice. The temperature at the orifice was determined from an average of two Chromel-constantan thermocouples. Orifice pressures were measured by calibrated transducers.

Radial surveys of the flow were made upstream of the inlet guide vanes (IGV's), between the IGV's and rotor, between the rotor and stator, and downstream of the stator. Two combination survey probes at each station were used to measure total pressure, total temperature, and flow angle. A photograph of the combination probe is shown in figure 5. Each probe was positioned with a null-balancing, stream-directional sensitive control system that automatically alined the probe to the direction of flow. The probes were angularly alined in an air tunnel. The thermocouple material was Chromel constantan.

The circumferential locations of the two survey probes, at each of the four measuring stations are shown in figure 6. The probes between the IGV's and rotor, and downstream of the stator were circumferentially traversed one blade passage counterclockwise from the nominal values shown. One IGV blade passage is 13.87° and one stator blade passage is 5.63°.

An electronic speed counter, in conjunction with a magnetic pickup, was used to measure rotative speed (rpm).

The estimated errors of the data based on inherent accuracies of the instrumentation and recording system are as follows:

Flow rate, kg/sec ±0.3
Rotative speed, rpm
Flow angle, deg
Temperature, K
Guide vane inlet total pressure, N/cm^2
Rotor inlet total pressure, N/cm^2
Rotor outlet total pressure, N/cm 2
Stator outlet total pressure, N/cm 2

Test Procedure

The stage survey data were taken at five weight flows ranging from maximum flow to the near-stall conditions at design speed. Data were recorded at 11 radial positions for each weight flow.

At each radial position the combination probes behind both the IGV's and stator were circumferentially traversed to nine different locations across the blade passages. Values of total pressure, total temperature, and flow angle were recorded at each circumferential position. At the last circumferential position, values of total pressure, total temperature, and flow angle were also recorded upstream of the IGV's and between the rotor and stator. All probes were then traversed to the next radial position and the circumferential traverse procedure repeated.

The back pressure on the stage was increased by closing the sleeve valve in the collector until a stalled condition was detected by a sudden drop in stage outlet total pressure. This pressure was measured by a probe located at mid-passage and was recorded on an X-Y plotter. Stall was corroborated with a sudden increase in noise level.

Calculation Procedure

Data was reduced using a streamline-analysis computer program which calculates all static pressures at each measuring station and flow angles at stations behind the rotating blade row. The inputs to this program include corrected weight flow, corrected speed, total pressure, and total temperature behind a rotating blade row and weight flow, total pressure, total temperature, and flow angle behind a fixed blade row. Static pressure is calculated within the program from considerations of continuity of mass flow and radial equilibrium which includes streamline curvature terms.

At each radial station nine circumferential values of total temperature, total pressure, and flow angle across both the IGV and stator gaps were area averaged to obtain

the IGV and stator values presented at each radial position.

The data, measured at the four measuring stations, have been translated to the blade leading and trailing edges by the method presented in reference 1.

Orifice weight flow, total pressure, static pressure and temperatures were all corrected to standard sea-level conditions based on the IGV inlet conditions.

RESULTS AND DISCUSSION

The results from this investigation are presented in three main sections. The overall performances for the rotor and the stage are presented first. Radial distributions of several performance parameters are then presented for the IGV's, rotor, and stator. Finally the blade-element data are presented for both the rotor and stator. The data presented are computer plotted; occasionally a data point falls outside the range of parameters shown in the figure and is omitted.

All of the plotted data together with some additional performance parameters are presented in tabular form. The overall performance data are presented in table VI. The blade element data are presented for the IGV, rotor, and stator in tables VII, VIII, and IX, respectively. The definitions and units used for the tabular data are presented in appendix C.

Overall Performance

The overall rotor performance is based on the data obtained between measuring stations 1 and 2 and overall stage performance is based on the data obtained between measuring stations 1 and 3 (see fig. 1). The overall performance for the rotor and for the stage, at the design blade tip speed of 425 meters per second, are presented in figures 7 and 8, respectively. Averaged values of total pressure ratio, total temperature ratio, and temperature rise efficiency are plotted as a function of equivalent weight flow. Data are presented at several weight flows over the stage stable operating flow range. Design point values are shown as solid symbols on both figures.

At a near design weight flow of 29.4 kilograms per second (195 (kg/sec)/m² of annulus area) the stage experimental overall temperature rise efficiency of 0.827 was 3.6 points lower than the value based on design losses. The experimental stage pressure ratio and temperature ratio were 1.48 and 1.14 as compared to the design values of 1.61 and 1.17. Peak efficiency for the stage was 0.830 and occurred at an equivalent weight flow of 28.8 kilograms per second. Stage pressure ratio at the peak efficiency point was 1.52.

The rotor experimental overall temperature rise efficiency of 0.85 at the near design weight flow of 29.4 kilograms per second was three points lower than the design value of 0.88. The rotor total pressure ratio and total temperature ratio were 1.52 and 1.15 as compared to the design values of 1.62 and 1.17. Rotor peak efficiency of 0.86 occurred at a pressure ratio of 1.56 and at a weight flow of 28.8 kilograms per second.

Stall margin for the stage was 8 percent based on equivalent weight flow and total pressure ratio at which peak efficiency occurred as compared with the values near stall.

Radial Distributions

Radial distribution of several flow and performance parameters at design speed are shown for the inlet guide vane, rotor, and stator in figures 9 to 11, respectively. The data shown represent the flow condition at near stall, peak efficiency, and choke. (Design values are shown by solid symbols.) Flow and performance results at the peak efficiency weight flow of 28.8 kilograms per second are compared with the design values.

Inlet guide vane. - The radial distribution of total loss coefficient for the inlet guide vanes (IGV's) is shown in figure 9. Substantial loss was recorded in the end wall regions. The compressor was designed without an IGV as previously noted. The IGV was designed and incorporated prior to testing. The aerodynamic design of the compressor therefore did not account for any loss associated with an IGV and the resulting total pressure profile entering the first stage rotor. In the design of the compressor a radially constant total pressure was assumed across the rotor inlet. A total boundary layer blockage of 2 percent was assumed in the design. It is noted that even ahead of the IGV inlet, a noticeable defect in total pressure exists at 5 percent of span as shown in the tabular data. This defect reflects an appreciable outer wall boundary layer entering the IGV.

Rotor. - The radial distributions of pressure ratio (fig. 10) at all weight flows is lower than design, particularly in the tip region where pressure ratio deteriorates rapidly. The total temperature ratio at peak efficiency weight flow is greater than design in the outer 50 percent of span and lower than design in the inner 50 percent of span. Resulting temperature rise efficiency in the tip region is considerably lower than design at all weight flows. The meridional velocity ratio deteriorates from 0.8 at 20 percent of span to 0.4 at 5 percent of span. The deviation angle gradient is very steep in the tip region with an accompanying rapid increase in loss. From this, it would appear that the rotor is stalling prematurely at the tip and limiting the range of the stage. This may, in part, be a result of what appears to be a relatively thick boundary layer entering the IGV coupled with the locally high losses through the IGV at the tip,

resulting in appreciably higher than design incidence angles (30) in the tip region.

With the rotor tip not passing the mass flow, a redistribution of flow within the blade passage took place. The blade passage between the damper and the hub passes additional weight flow as indicated by the meridional velocity ratio distribution. The higher meridional velocity ratio apparently unloads the inner 50 percent of the blade as indicated by the diffusion-factor distribution. The deviation angle in the hub region has a sharp gradient. This is not reflected in the design values which were based on a modification of Carter's Rule.

An appreciable defect in pressure ratio and efficiency was noted in the damper region resulting in gradients in flow parameters entering the stator. Aerodynamic design of this rotor did not account for these effects.

It appears that the rotor did not meet its design flow as a result of premature tip stalling and damper effects.

Stator. - The reduced flow in the rotor tip resulted in very high incidence angles at the stator tip (fig. 11). The higher than design flow between rotor damper and hub resulted in low incidence angles to the stator. Stator losses are high from 30 percent of span to the hub.

Variation with Incidence Angle

The variations of selected blade-element performance parameters are presented as a function of incidence angle in figure 12 for the rotor and in figure 13 for the stator. The data are presented at design speed for the blade-element locations of 5, 10, 30, 50, 70, 90, and 95 percent of blade span from the rotor outlet blade tip. Design values are shown by solid symbols. The incidence angle curves are presented primarily for future use in comparing the performance of these blades with other blade designs. Thus, only a few brief observations will be made from the curves at present.

Rotor. - In both the hub and tip region of the blade, incidence angles were greater than the design value of 0° over the whole flow range of the stage. The meridional velocity ratio was greater than design at 70, 90, and 95 percent of span and considerably less than design at 5 percent span. Apparently there is a radial shift in the flow away from the rotor tip. The diffusion factor at all elements were less than design at design incidence. The losses at design incidence were greater or equal to design at all elements except at 90 percent of span. At 5 percent span and decreasing incidence angle the increase in loss parameter at 1° incidence angle while loss coefficient continues to decrease is attributed to an abrupt decrease in rotor outlet relative meridional flow angle.

Stator. - As a result of the radial flow shift occurring through the rotor the stator

blading is operating at incidence angles considerably off design across the entire blade span except at 10 and 30 percent of span. Absolute values of minimum loss were less than design in both the hub and tip region. Minimum loss occurred at incidence angles greater than design at 5 and 10 percent of span, near design at 30 and 50 percent of span, and less than design at 70, 90, and 95 percent of span.

SUMMARY OF RESULTS

This report has presented both the aerodynamic design parameters and the overall and blade-element performance of the first stage of a transonic multistage compressor. Detailed radial surveys of the flow conditions in front of the IGV's, between the IGV's and the rotor, between the rotor and stator and behind the stator were made over the stage stable operating flow range at design speed. Flow and performance parameters were calculated across 11 radial positions. The following principal results were obtained:

- 1. At design speed, the stage peak efficiency of 0.83 occurred at a pressure ratio of 1.52 and a weight flow of 28.8 kilograms per second.
- 2. Rotor peak efficiency of 0.86 occurred at a pressure ratio of 1.56 and at a weight flow of 28.8 kilograms per second.
- 3. Stage stall margin was 8 percent based on pressure ratio and weight flow at the peak efficiency and stall conditions.
- 4. The rotor tip appears to be stalling prematurely as evidenced by high rotor tip losses, high deviation angles, and low velocity ratios.
- 5. Premature stalling of the rotor tip appears to limit the flow range of the stage. Large boundary layer in the rotor tip region and gradients due to the rotor damper result in severe gradients at the stator inlet.

Lewis Research Center,

National Aeronautics and Space Administration, Cleveland, Ohio, October 8, 1975, 505-04.

APPENDIX A

SYMBOLS

	·
A _{an}	annulus area at rotor leading edge, m ²
$\mathbf{A_f}$	frontal area at rotor leading edge, m ²
C _p	specific heat at constant pressure, 1004 J/(kg)(K)
D	diffusion factor
i _{mc}	mean incidence angle, angle between inlet air direction and line tangent to blade mean camber line at leading edge, deg
i _{ss}	suction-surface incidence angle, angle between inlet air direction and line tangent to blade suction surface at leading edge, deg
N	rotative speed, rpm
P	total pressure, N/cm ²
p	static pressure, N/cm ²
r	radius, cm
SM	stall margin
Т	total temperature, K
U	wheel speed, m/sec
v	air velocity, m/sec
W	weight flow, kg/sec
\mathbf{Z}	axial distance referenced from rotor blade hub leading edge, cm
$^{lpha}{_{ m c}}$	cone angle, deg
$lpha_{f s}$	slope of streamline, deg
β	air angle (angle between air velocity and axial direction), deg
$eta_{f c}^{m \cdot}$	relative meridional air angle based on cone angle, $\arctan{(\tan{\beta_m^*}\cos{\alpha_c}/\cos{\alpha_s})}$ deg
γ	ratio of specific heats
δ	ratio of rotor-inlet total pressure to standard pressure of 10.13 N/cm ²
$\delta^{\mathbf{O}}$	deviation angle, angle between exit air direction and tangent to blade mean camber line at trailing edge, deg

 θ ratio of rotor inlet total temperature to standard temperature of 288.2 K

η efficiency

 κ_{mc} angle between blade mean camber line and meridional plane, deg

 κ_{ss} angle between blade suction-surface camber line at leading edge and meridional

plane, deg

σ solidity, ratio of chord to spacing

 $\overline{\omega}$ total loss coefficient

 $\overline{\omega}_n$ profile loss coefficient

 $\overline{\omega}_{\rm s}$ shock loss coefficient

Subscripts:

ad adiabatic (temperature rise)

id ideal

LE blade leading edge

m meridional direction

mom momentum-rise

p polytropic

TE blade trailing edge

z axial direction

 θ tangential direction

o instrumentation plane upstream of inlet guide vanes

1 instrumentation plane upstream of rotor

2 instrumentation plane between rotor and stator

3 instrumentation plane downstream of stator

Superscript:

relative to blade

APPENDIX B

EQUATIONS

Suction-surface incidence angle -

$$i_{SS} = \left(\beta_C^{\dagger}\right)_{I,E} - \kappa_{SS} \tag{B1}$$

Mean incidence angle -

$$i_{mc} = \left(\beta_c^{\dagger}\right)_{LE} - \left(\kappa_{mc}\right)_{LE} \tag{B2}$$

Deviation angle -

$$\delta^{O} = \left(\beta_{\mathbf{c}}^{\prime}\right)_{\mathbf{TE}} - \left(\kappa_{\mathbf{mc}}\right)_{\mathbf{TE}} \tag{B3}$$

Diffusion factor -

$$D = 1 - \frac{\mathbf{V_{TE}'}}{\mathbf{V_{LE}'}} + \left| \frac{\left(\mathbf{rV_{\theta}} \right)_{\mathbf{TE}} - \left(\mathbf{rV_{\theta}} \right)_{\mathbf{LE}}}{(\mathbf{r_{TE}} + \mathbf{r_{LE}})\sigma(\mathbf{V_{LE}'})} \right|$$
(B4)

Total loss coefficient -

$$\overline{\omega} = \frac{\left(P'_{id}\right)_{TE} - P'_{TE}}{P'_{LE} - P_{LE}}$$
(B5)

Profile loss coefficient -

$$\overline{\omega}_{p} = \overline{\omega} - \overline{\omega}_{s}$$
 (B6)

Total loss parameter -

$$\frac{\overline{\omega}\cos\left(\beta_{\mathbf{m}}^{\prime}\right)_{\mathbf{TE}}}{2\sigma}\tag{B7}$$

Profile loss parameter -

$$\frac{\overline{\omega}_{p} \cos \left(\beta_{m}^{\prime}\right)_{TE}}{2\sigma} \tag{B8}$$

Adiabatic (temperature rise) efficiency -

$$\eta_{\text{ad}} = \frac{\left(\frac{P_{\text{TE}}}{P_{\text{LE}}}\right)^{(\gamma-1)/\gamma} - 1}{\frac{T_{\text{TE}}}{T_{\text{LE}}} - 1}$$
(B9)

Momentum-rise efficiency -

$$\eta_{\text{mom}} = \frac{\left(\frac{\mathbf{P}_{\text{TE}}}{\mathbf{P}_{\text{LE}}}\right)^{(\gamma-1)/\gamma} - 1}{\frac{\left(\mathbf{U}\mathbf{V}_{\theta}\right)_{\text{TE}} - \left(\mathbf{U}\mathbf{V}_{\theta}\right)_{\text{LE}}}{\mathbf{T}_{\text{LE}}\mathbf{C}_{\mathbf{p}}}} \tag{B10}$$

Equivalent weight flow -

$$\frac{\mathbf{w}\sqrt{\theta}}{\delta}$$
 (B11)

Equivalent rotative speed -

$$\frac{N}{\sqrt{\theta}}$$
 (B12)

Weight flow per unit annulus area -

$$\frac{\left(\frac{\mathbf{W}\sqrt{\theta}}{\delta}\right)}{\mathbf{A}_{\mathbf{an}}} \tag{B13}$$

Weight flow per unit frontal area -

$$\frac{\left(\frac{\mathbf{W}\sqrt{\theta}}{\delta}\right)}{\mathbf{A_f}} \tag{B14}$$

Head-rise coefficient -

$$\frac{C_{p}T_{LE}}{U_{tip}^{2}}\left[\left(\frac{P_{TE}}{P_{LE}}\right)^{(\gamma-1)/\gamma} - 1\right]$$
(B15)

Flow coefficient -

$$\left(\frac{V_z}{U_{tip}}\right)_{LE}$$
 (B16)

Stall margin -

$$SM = \frac{\left(\frac{P_{TE}}{P_{LE}}\right)_{stall} \times \left(\frac{W\sqrt{\theta}}{\delta}\right)_{ref}}{\left(\frac{P_{TE}}{P_{LE}}\right)_{ref}} \times \frac{\left(\frac{W\sqrt{\theta}}{\delta}\right)_{ref}}{\left(\frac{W\sqrt{\theta}}{\delta}\right)_{stall}} - 1$$
(B17)

Polytropic efficiency -

$$\eta_{p} = \frac{\ln\left(\frac{P_{TE}}{P_{LE}}\right)^{(\gamma-1)/\gamma}}{\ln\left(\frac{T_{TE}}{T_{LE}}\right)}$$
(B18)

APPENDIX C

DEFINITIONS AND UNITS USED IN TABLES

ABS absolute

AERO CHORD aerodynamic chord, cm

AREA RATIO ratio of actual flow area to critical area (where local Mach number

is one)

BETAM meridional air angle, deg

CONE ANGLE angle between axial direction and conical surface representing blade

element, deg

DELTA INC difference between mean camber blade angle and suction-surface

blade angle at leading edge, deg

DEV deviation angle (defined by eq. (B3)), deg

D-FACT diffusion factor (defined by eq. (B4))

EFF adiabatic efficiency (defined by eq. (B9))

IN inlet (leading edge of blade)

INCIDENCE incidence angle (suction surface defined by eq. (B1) and mean defined

by eq. (B2)), deg

KIC angle between the blade mean camber line at the leading edge and the

meridional plane, deg

KOC angle between the blade mean camber line at the trailing edge and the

meridional plane, deg

KTC angle between the blade mean camber line at the transition point and

the meridional plane, deg

LOSS COEFF loss coefficient (total defined by eq. (B5) and profile defined by

eq. (B6))

LOSS PARAM loss parameter (total defined by eq. (B7) and profile defined by

eq. (B8))

MERID meridional

MERID VEL R meridional velocity ratio

OUT outlet (trailing edge of blade)

PERCENT SPAN percent of blade span from tip at rotor outlet

PHISS suction-surface camber ahead of assumed shock location, deg

PRESS pressure, N/cm²

PROF profile

RADII radius, cm

REL relative to blade

RI inlet radius (leading edge of blade), cm

RO outlet radius (trailing edge of blade), cm

RP radial position

RPM equivalent rotative speed, rpm

SETTING ANGLE angle between aerodynamic chord and meriodional plane, deg

SOLIDITY ratio of aerodynamic chord to blade spacing

SPEED speed, m/sec

SS suction surface

STREAMLINE SLOPE slope of streamline, deg

TANG tangential

TEMP temperature, K

TI thickness of blade at leading edge, cm

TM thickness of blade at maximum thickness, cm

TO thickness of blade at trailing edge, cm

TOT total

TOTAL CAMBER difference between inlet and outlet blade mean camber lines, deg

VEL velocity, m/sec

WT FLOW equivalent weight flow, kg/sec

X FACTOR ratio of suction-surface camber ahead of assumed shock location

of multiple-circular-arc blade section to that of double-

circular-arc blade section

ZIC axial distance to blade leading edge from inlet, cm

ZMC axial distance to blade maximum thickness point from inlet, cm

ZOC axial distance to blade trailing edge from inlet, cm

ZTC axial distance to transition point from inlet, cm

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TABLE I. - DESIGN OVERALL PARAMETERS FOR

STAGE 66

ROTOR TOTAL PRESSURE RATIO	1.621
STAGE TOTAL PRESSURE RATIO	1.606
•	
ROTOR TOTAL TEMPERATURE RATIO	1.168
STAGE TOTAL TEMPERATURE RATIO	1.168
ROTOR ADIABATIC EFFICIENCY	0.881
STAGE ADIABATIC EFFICIENCY	0.863
ROTOR POLYTROPIC EFFICIENCY	0.888
	0.871
	7
ROTOR HEAD RISE COEFFICIENT	0.237
STAGE HEAD RISE COEFFICIENT FLOW COEFFICIENT	0.232
FLOW COEFFICIENT	0.464
WT FLOW PER UNIT FRONTAL AREA 1	47.469
WT FLOW PER UNIT ANNULUS AREA	97.021
NT FLOW	29.710
RPM 160	42.300
	25.426
111 J. CLD	LJ.4L0

TABLE II. - DESIGN BLADE-ELEMENT PARAMETERS FOR ROTOR 66

10	25.324	24.657 24.657 24.092 22.962 21.831 20.927 20.023 19.571 17.310 16.180 15.049	0. 0. 0. 0. 0.	42.7 42.2 41.3 41.0 41.3 41.9 42.3 44.8 46.6 48.6	64.5 63.8 62.4 60.9 59.8 58.7 58.1 55.1	BETAM 0UT 63.5 62.4 61.4 59.2 56.7 54.3 51.7 50.1 40.3 33.2 24.2 18.9 13.2	TOTA 1N 288.2 288.2 288.2 288.2 288.2 288.2 288.2 288.2 288.2 288.2 288.2	1.177 1.169 1.165 1.162 1.161 1.158 1.157 1.158	IN 10.13 10.13 10.13 10.13 10.13 10.13 10.13 10.13 10.13	RATIO 1.621 1.621 1.621 1.621 1.621 1.621 1.621 1.621 1.621 1.621 1.621
RP TIP 1 2 3 4 5 6 7 8 9 10 11 HUB	ABS 1N 196.6 198.4 200.1 202.8 203.8 203.0 202.4 197.3 193.5 186.5 184.2	VEL 0UT 197.5 198.6 199.6 199.6 201.1 203.3 206.0 209.1 211.0 222.7 231.5 247.6 254.0	405.5 390.8 383.4 344.5 324.0 302.8 291.8	0UT 322.3 315.2 308.3 294.6 279.4 265.3 250.7 243.3 207.1 189.9 175.1 169.6	1N 196.6 198.4 200.1 202.6 203.8	151.1 153.5	IN .0.	135.3 134.8 134.2 132.8 134.2 132.8 135.3 136.0 139.8 142.1 156.9 167.7 181.2 188.5 196.0	IN 425.4 416.5 406.8 387.1 366.9	404.7 385.7 366.8
RP TIP 1 2 3 4 5 6 7 8 9	0.610	0UT 0.546 0.550 0.555 0.562 0.570 0.579 0.590 0.632 0.638 0.690 0.709	IN 1.426 1.405 1.381 1.332 1.280 1.237 1.192 1.169 1.048 0.985 0.919	0UT 0.891 0.874 0.857 0.823 0.784 0.746 0.707 0.588 0.541 0.500 0.486	IN 0.598 0.604 0.610 0.618 0.622 0.622 0.617 0.601 0.588 0.573	0UT 0.398 0.404 0.411 0.422 0.431 0.435 0.439 0.440 0.448 0.452 0.457 0.460	IN -3.94 -3.63 -3.19 -1.87 -0.06 1.63 3.47 4.45 9.90 13.05 16.51 18.39	0UT -4.94 -4.14 -3.31 -1.56 0.36 1.98 3.68 4.56	VEL R 0.732 0.735 0.738 0.746 0.753 0.759 0.766 0.770 0.800 0.845 0.861	MACH NO 1.524 1.514 1.504 1.483 1.463 1.450 1.459 1.434 1.418 1.410 1.340 1.298
RP TIP 1 2 3 4 5 6 7 8 9 10 11 HUB	PERCENT SPAN 0. 5.00 10.00 20.00 30.00 38.00 46.00 50.00 70.00 80.00 90.00 95.00	MEAN 2.7 2.9 3.2	0.0 -0.0 0.0 0.0	4.5 4.0 3.7 3.6 3.6 3.7 4.7 5.6	0.416 0.419 0.421 0.425 0.433 0.445 0.460 0.468 0.510	0.747 0.767 0.789 0.836 0.877 0.896 0.911 0.917 0.939 0.940 0.936	10T 0.198 0.181 0.164 0.127 0.097 0.084 0.074	0EFF PROF 0.108 0.097 0.086 0.060 0.041 0.036 0.034 0.037 0.048 0.070 0.087	LOSS P. TOT 0.032 0.029 0.027 0.017 0.014 0.012 0.014 0.015 0.015	PROF 0.017 0.016 0.014 0.010 0.007 0.006 0.006 0.007 0.009 0.013 0.014

TABLE III. - DESIGN BLADE-ELEMENT PARAMETERS FOR STATOR 66

RP TIP 1 2 3 4 5 6 7 8 9 10 11 HUB	RAD I IN 24.968 2 24.447 2 23.937 2 21.886 2 21.063 2 21.063 2 21.7767 1 16.739 1 15.717 1 15.717 1	OUT 25.121 24.358 25.897 22.970 22.970 22.038 21.290 21.290 20.172 18.326 17.412 66.499 16.040	ASS 1N 39.6 39.2 38.8 38.0 37.7 38.6 39.0 41.3 43.0 44.9 45.4	٥.	IN 39.6 39.2 38.8 38.0 37.7 38.0 38.6 39.0	0.	1N 345.2 343.7 342.2 339.1 336.8 335.7 334.6 333.6 333.5 333.7 333.8	L TEMP RATIO 1.003 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000	IN 16.42 16.42 16.42 16.42 16.42 16.42 16.42	0.994 0.993 0.991 0.988 0.980 0.972
5 6 7 8 9	215.0 215.5 216.3 217.6 219.4 221.5 222.9 231.5 237.8 245.9 250.5	0UT ! 174.3 176.1 177.0 177.8 177.8 177.7 177.3 177.0 174.3 170.9 165.0	IN 214.3 215.0 215.5 216.3 217.6 219.4 221.5 222.9 231.5 237.8 245.9	VEL 0UT 174.3 176.1 177.8 177.7 177.3 177.0 174.3 1765.0 161.0 155.8	MERI IN 165.0 166.5 168.0 170.6 172.2 173.1 173.2 173.8 174.0 174.3	0UT 174.3 176.1 177.0 177.8	IN 136.7 135.9 135.0 133.1 132.9 135.1 138.3 140.2	0. 0. 0.	IN 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	0. 0. 0. 0. 0. 0.
RP TIP 1 2 3 4 5 6 7 8 9 10 11 HUB	0.595 0.599 0.602 0.607 0.613 0.620 0.627 0.632 0.659 0.679 0.704 0.719	OUT 0.478 0.485 0.489 0.493	IN 0.595 0.599 0.602 0.607 0.613 0.620 0.627 0.632 0.659 0.679	ACH NO OUT 0.478 0.485 0.485 0.495 0.495 0.495 0.495 0.495 0.478 0.468 0.448	IN 0.459 0.464 0.469 0.479 0.486 0.488 0.490 0.491 0.495 0.497	OUT	-3.54 -2.48 -1.49 0.35 2.03 3.33 4.64 5.32 8.93	OUT -2.24 -0.99 -0.25 1.18 2.56 3.68 4.84 5.44 8.61 10.35	VEL R 1.056 1.057 1.054	MACH NO 0.962 0.956 0.949 0.935 0.930 0.936 0.947
RP TIP 1 2 3 4 5 6 7 8 9 10 11 HU5	PERCENT SPAN 0. 5.00 10.00 20.00 30.00 38.00 46.00 50.00 70.00 80.00 90.00 95.00	INC II MEAN 4.0 3.9 3.7 3.5 3.3 3.2 2.6 2.4 2.7	DENCE SS -3.0 -2.9 -2.8 -2.5 -2.3 -2.1 -1.9 -1.5 -1.3 -1.1 -1.0	DEV 8.7 8.2 7.8 7.5 7.5 7.5 7.7 8.0 8.0	0.401 0.389 0.381 0.368 0.362 0.364 0.369 0.373 0.403	0. 0. 0.	LOSS CO TOT 0.115 0.045 0.029 0.026 0.027 0.028 0.028 0.028 0.045 0.045 0.071 0.096	DEFF PROF 0.115 0.045 0.029 0.026 0.027 0.028 0.028 0.034 0.045 0.071 0.096 0.130	LOSS P TOT 0.039 0.015 0.011 0.009 0.008 0.008 0.008 0.008 0.008 0.010 0.015 0.020	ARAM PROF 0.039 0.011 0.009 0.008 0.008 0.008 0.008 0.008 0.010 0.015 0.026

TABLE IV. - BLADE GEOMETRY FOR ROTOR 66

```
PERCENT
                                BLADE ANGLES
               RADII
                                                   DELTA
                                                           CONE
       SPAN .
             RI
                    · R0
                              KIC
                                     KTC
                                            KOC
                                                    INC
                                                           ANGLE
         0. 25.324 25.222
TIP
                             62.51
                                    63.11
                                           58.81
                                                          ~3.238
                                                    2.68
         5. 24.794 24.657
                             61.59
                                    62.04
                                           57.92
                                                    2.93
                                                          -4.225
        10. 24.216 24.092
                             60.60
                                    60.87
                                           57.03
                                                    3.20
                                                          -3.688
        20. 23.041 22.962
                             58.61
                                           55.18
                                    58.47
                                                    3.75
                                                          -2.213
        30. 21.841 21.831
                             56.67
                                    55.94
                                           52.98
                                                    4.27
                                                          -0.268
        38. 20.866 20.927
                             55.14
                                    53.75
                                           50.75
                                                    4.69
                                                           1.522
        46. 19.878 20,023
                             53.63 51.48
                                           48.06
                                                    5.07
                                                          3.444
        50. 19.378 19.571
                                    50.29
                                                    5.26
                             52.87
                                           46.46
                                    44.21
        70. 16:811 17.310
                             48.96
                                           35.52
                                                    6.08
                                                          10.070
                                                    6.39
6.59
        80. 15.470 16.180
                             46.91
                                    40.93
                                           27.52
                                                          13.261
                             44.75
        90. 14.079 15.049
                                    37.49
                                           17.34
10
                                                          16.722
11
        95. 13.361 14.484
                             43.60
                                    35.80
                                           11.47
                                                    6.65
                                                          18.571
       100. 12.700 13.919
                                    34.26
                                          - 5.34
HUB -
                             42.52
                                                    6.68
                                                          19,462
       BLADE THICKNESSES
                                  AXIAL DIMENSIONS
                             ZIC
RP
       Ti
              TM
                     TO
                                     ZMC
                                            ZTC
                                                    ZOC
      0.025
             0.115
                    0.025
                             0.808 1.689
                                           1.936
                                                  2.604
                             0.778
                                           1.910
                                    1.688
                                                   2.636
      0.028
             0.126 0.028
      0.030
             0.138
                    0.030
                             0.746
                                    1.687
                                           1.879
                                                   2.667
      0.035
             0.161
                    0.035
                             0.681
                                    1.684 1.809
                                                   2.730
                             0.615
      0.041
             0.184
                     0.041
                                    1.680
                                           1,726
                                                   2.795
      0.044
                     0.044
                             0.561
                                    1.677
                                          1.650
             0.202
                                                   2.852
      0.048
                     0.048
             0.218
                             0.505
                                    1.672
                                           1.565
                                                   2,913
      0.050
             0.227
                     0.050
                             0.476
                                    1.670
                                           1.518
                                           1.244
      0.059
             0.265
                     0.059
                             0.320
                                    1.650
                                                   3.130
      0.062
             0.282
                     0.062
                             0.226
                                    1.635
                                           1.075
                                                   3.237
      0.066
             0.298
                     0.066
                             0.117
                                    1.616
                                           0.879
11
      0.068
                             0.057
                                   1.606
                                                   3.399
             0.305
                     0.068
                                           0.772
HUB
      0.069
             0.312
                     0.069
                             0.000
                                    1.596 0.672
            SETTING TOTAL
      AER0
             ANGLE CAMBER SOLIDITY FACTOR PHISS
      CHORD
                                                    CITAR
      3.875
                             1.391
                                                    1.045
TIP
                     3.70
                                    0.592
                                           2.83
             62.15
1
      3.884
             61.13
                     3.67
                             1.425
                                    0.641
                                             3.19
                                                    1.040
      3.884
             60.03
                     3.58
                             1,459
                                   0.693
                                            3.58
                                                    1.034
                             1.531
                                            4.35
      3.882
             57.79
                     3.43
                                    0.788
      3.881
             55.42
                     3.69
                             1.613
                                    0.868
                                            5.19
                                                    1.014
                                            5.96
      3.882
             53.32
                     4.39
                             1.685
                                    0.921
                                                    1.007
                     5.57
                             1.766
                                    0.961
                                            6.76
      3.884
             51.04
                                             7.17
      3.886
             49.78
                     6.41
                             1.810
                                    0.977
                                                    1.003
      3.914
             42.24
                     13.44
                             2.081
                                    1.002
                                            9.03
                                                    0.997
      3.947
                     19:39
                                            9.90
             37.23
                             2.263
                                    1.000
                                                    0.999
      4.003
             31.06
                    27.41
                             2.494
                                    1.000
                                           10.69
                                                    1.005
      4.044
             27.55
                    32.13
                             2.635
                                    1.000
                                           10.94
                                                    1.009
11
      4.073
             23.95
                     37.18
                             2.776
                                    1.000
                                           11,13
                                                    1.013
```

TABLE V. - BLADE GEOMETRY FOR STATOR 66

RP TIP 1 2 3 4 5 6 7 8 9 10 HUB	PERCENT RADII SPAN Ri RO 0. 24.968 25.121 5. 24.447 24.358 10. 23.937 23.897 20. 22.913 22.970 30. 21.886 22.038 38. 21.063 21.290 46. 20.240 20.544 50. 19.827 20.172 70. 17.767 18.326 80. 16.739 17.412 90. 15.715 16.499 95. 15.207 16.040 100. 14.834 15.494	35.39 21.72 35.05 21.85 34.29 22.08 34.18 22.54 34.68 23.15 35.41 23.15 35.86 24.32 38.55 26.75 40.37 28.31	KOC INC -8.65 7.04 -8.37 6.76 -8.18 6.53 -7.79 6.76 -7.51 5.45 -7.52 5.13 -7.53 4.97 -7.66 4.23 -7.79 3.57 -8.02 3.42	CONE ANGLE 2.507 -1.470 -0.657 0.944 2.481 3.716 4.985 5.642 9.148 11.009 12.824 13.652 10.909
	BLADE THICKNESSES	AXIAL D	IMENICIONS	٠.
RP	TI TM TO	ZIC ZMC	ZTC ZOC	
TIP	0.065 0.297 0.067	6.042 7.700	7.068 9.523	
i	0.064 0.286 0.064	6.040 7.701		
2 3	0.062 0.276 0.062 0.057 0.261 0.057	6.037 7.701 6.032 7.703		_
3	0.054 0.243 0.054	6.031 7.703	6.932 9.527	
5 6	0.051 0.230 0.051 0.048 0.217 0.048		6.912 9.529	4
7	0.047 0.211 0.047	6.039 7.702 6.042 7.702	6.896 9.531 6.889 9.531	
8	0.040 0.182 0.040	6.061 7.699	6.855 9.534	
9 10	0.037 0.169 0.037 0.035 0.156 0.035	01:0:0	6.841 9.535 6.828 9.535	
ij	0.033 0.151 0.033	6.102 7.693		•
HUB	0.032 0.147 0.032	6.109 7.693		
	v			
RP	AERO SETTING TOTAL CHORD ANGLE CAMBER S	ALIDITY EACTOR	AREA R PHISS RATIO	•
TIP	3.650 13.53 44.32		18.33 1.139	
1	3.648 13.51 43.75	1.523 1.000	17.64 1.149	
2	3.647 13.44 43.24 3.647 13.25 42:07	1.553 1.000		
3 4	3 650 13 31 41 74	1.693 1.000	14.69 : 1.180	
5	3.654 13.58 42.19 3.660 13.95 42.93	1.758 1.000	14.34 1.187 14.12 1.193	-
5 6 7	3.660 13.95 42.93 3.663 14.17 43.39	1.828 1.000		
8	3.690 15.44 46:21	2.083 1.000	13.81 1.207	·
9 10	3.709 16.29 48.16 3.732 17.25 50.42	2.213 1.000 2.360 1.000	13.87 1.216 13.99 1.227	
11	3.743 17.72 51.49	2.440 1.000	14.00 1.231	•
HUB	3.702 18.06 52.30	2.487 1.000	14.00 1.234	

TABLE VI. - OVERALL PERFORMANCE FOR STAGE 1

(100 PERCENT OF DESIGN SPEED)

Parameter		Rea	ding Num	ber	
	845	856	867	884	895
ROTOR TOTAL PRESSURE RATIO	1.591	1.581	1.553	1.517	1,445
STAGE TOTAL PRESSURE RATIO	1.558	1.548	1.518	1.478	1.392
ROTOR TOTAL TEMPERATURE RATIO	1.166	1,163	1.157	1,149	1,135
STAGE TOTAL TEMPERATURE RATIO	1.166	1.161	1.153	1,143	1.125
ROTOR ADIABATIC EFFICIENCY	0.853	0.855	0.855	0.847	0.822
STAGE ADIABATIC EFFICIENCY	0.813	0.823	0.830	0.827	0.790
ROTOR POLYTROPIC EFFICIENCY	0.863	0.864	0.864	0.856	0.831
STAGE POLYTROPIC EFFICIENCY	0.825	0.834	0.840	0.836	0.800
ROTOR HEAD RISE COEFFICIENT	0.228	0.224	0.216	0.201	0.176
STAGE HEAD RISE COEFFICIENT	0.217	0.213	0.204	0.188	0.157
FLOW COEFFICIENT	0.395	0.406	0.416	0.426	0.434
**EQUIVALENT VALUES BASED ON STAGE INLET*	1			20.40	
WEIGHT FLOW	27.78	28.38	28.81	29.40	29.82
WEIGHT FLOW PER UNIT ANNULUS AREA	184.23	188.18	191.08	194.99 145.95	197.76
WEIGHT FLOW PER UNIT FRONTAL AREA WHEEL SPEED. RPM	137.90	140.85	143.02	16072.0	148.03
TIP SPEED	424.5	16037.4 425.3	15986.6	426.2	16091.2 426.7
PERCENT OF DESIGN SPEED	99.8	100.0	423.9	100.2	100.3
CUMULATIVE VALUES	33.0	100.0	99.7.		100.5
COMPRESSOR TOTAL PRESSURE RATIO	1.549	1.538	1,508	1,467	1.381
COMPRESSOR TOTAL TEMPERATURE RATIO	1.169	1.165	1,156	1,146	1,129
COMPRESSOR ADIABATIC EFFICIENCY	0.788	0.795	0.799	0.794	0.752
COMPRESSOR POLYTROPIC EFFICIENCY	0.801	0.808	0.810	0.804	0.763

TABLE VII. - BLADE-ELEMENT DATA AT BLADE EDGES FOR INLET GUIDE VANE

(a) Reading 845

RP 1 2 3 4 5 6 7 8 9 10	RADII IN OUT 25.072 24.971 24.412 24.354 23.058 23.096 21.659 21.806 20.508 20.752 19.334 19.682 18.738 19.139 15.624 16.350 13.960 14.889 12.192 13.365 11.255 12.573	ABS BETAM IN OUT -2.0 -0.1 -1.5 01.1 10.8 0.1 0.5 0.1 1.5 0. 2.3 -0. 2.5 0.8 1.9 1.4	5 -1.5 0.3 5 -1.1 1.3 9 -0.8 0.9 9 0.5 0.9 0.1 0.8 7 1.5 0.7 5 2.3 -0.3 2.5 0.3 2.1 0.8	TOTAL TEMP IN RATIO 289.1 1.002 288.8 1.003 288.7 1.003 287.9 1.003 287.9 1.002 287.9 1.002 287.5 1.002 287.5 1.002 287.6 1.002 288.5 1.001	TOTAL PRESS IN RATIO 10.04 0.989 10.14 0.995 10.14 0.995 10.14 0.996 10.14 0.996 10.14 0.996 10.14 0.996 10.14 0.994 10.14 0.994 10.14 0.993 10.14 0.998
RP 1 2 5 4 5 6 7 8 9 11 1	ABS VEL IN OUT 141.9 156.0 147.8 163.3 150.7 167.3 150.0 167.2 149.8 167.6 149.0 167.1 148.5 166.7 144.4 162.2 141.5 158.7 137.9 153.5 135.8 148.8	REL VEL IN 0UT 141.9 156.0 147.8 163.3 150.7 167.3 150.0 167.2 149.8 167.6 149.0 167.1 148.5 166.7 144.4 162.2 141.5 158.7 137.9 153.5 135.8 148.8	MERID VEL IN OUT 141.8 155.9 147.8 163.3 150.7 167.2 149.9 167.2 149.8 167.6 149.0 167.1 148.4 166.7 144.2 162.2 141.4 158.7 137.8 153.5 135.7 148.7	TANG VEL IN OUT -5.0 -1.4 -3.7 0.9 -2.9 3.8 -2.1 2.7 1.2 2.6 0.3 2.3 3.9 2.0 5.9 -1.0 6.1 0.8 5.2 2.1 4.6 3.5	WHEEL SPEED IN OUT 0.
RP 1 2 3 4 5 6 7 8 9 10 11	ABS MACH NO IN OUT 0.424 0.467 0.442 0.490 0.451 0.502 0.449 0.503 0.449 0.504 0.447 0.503 0.445 0.502 0.432 0.488 0.424 0.477 0.412 0.460 0.405 0.445	REL MACH NO IN OUT 0.424 0.467 0.442 0.490 0.451 0.502 0.449 0.503 0.449 0.503 0.445 0.502 0.432 0.488 0.424 0.477 0.412 0.460 0.405 0.445	MERID MACH NO IN OUT 0.423 0.467 0.442 0.490 0.451 0.502 0.449 0.503 0.449 0.504 0.447 0.503 0.445 0.502 0.445 0.405 0.405 0.445	· .	MERID PEAK SS VEL R MACH NO 1.100 0.424 1.105 0.442 1.110 0.451 1.115 0.449 1.119 0.449 1.121 0.447 1.123 0.445 1.124 0.432 1.123 0.424 1.114 0.412 1.096 0.405
RP 1 2 3 4 5 6 7 8 9 10 11	PERCENT INCI SPAN MEAN 5.00 -2.0 10.00 -1.5 20.00 -1.1 30.00 -0.8 38.00 0.5 46.00 0.1 50.00 1.5 70.00 2.3 80.00 2.4 90.00 2.1 95.00 1.9	DENCE DEV SS -14.0 -0.5 -13.5 0.3 -13.1 1.3 -12.8 0.9 -11.5 0.9 -11.9 0.8 -10.5 0.7 -9.7 -0.3 -9.6 0.3 -9.9 0.8 -10.1 1.4	D-FACT EFF -0.086 00.089 00.089 00.101 00.115 00.116 00.118 00.108 00.108 00.108 00.108 0.	LOSS COEFF TOT PROF 0.095 0.095 0.042 0.044 0.037 0.037 0.029 0.029 0.030 0.030 0.030 0.030 0.047 0.047 0.054 0.054 0.066 0.066 0.109 0.109	LOSS PARAM TOT PROF 0.048 0.048 0.021 0.021 0.021 0.021 0.016 0.016 0.012 0.012 0.012 0.012 0.011 0.011 0.015 0.015 0.016 0.016 0.017 0.017 0.026 0.026

TABLE VII. - Continued.

(b) Reading 856

RP 1 2 3 4 5 6 7 8 9 10 11	RADII 1N 0UT 25.072 24.971 24.412 24.354 23.058 23.096 21.659 21.806 20.508 20.752 19.334 19.682 18.738 19.682 15.624 16.350 13.960 14.889 12.192 13.365 11.255 12.573	IN -2.2 -1.4 -1.0 -0.1 +0.2 1.3 1.4 1.5 2.5	BETAM OUT -0.5 0.0 0.9 0.7 0.8 0.7 -0.6 -0.1	IN -2.2 -1.4 -1.0	BETAM OUT -0.5 0.0 0.9 0.7 0.8 0.7 0.7 -0.6 -0.1 0.9	TOTA (N 289.1 288.8 288.5 288.0 287.9 287.7 287.7 288.0 288.5	I. TEMP RATIO 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.002 1.002	TOTAL IN 10.05 10.15 10.14 10.14 10.14 10.14 10.14 10.14	PRESS RATIO 0.990 0.994 0.995 0.996 0.996 0.993 0.993 0.993
RP 1 254 567 8 9 1 1 1	ABS VEL IN OUT 145.2 161.4 151.5 168.3 154.5 172.2 153.6 172.1 153.4 172.4 152.7 171.9 152.3 171.4 148.5 166.8 145.5 163.1 141.8 157.2 139.5 152.1	REL 15.2 151.5 154.5 153.6 153.4 152.7 152.3 148.5 141.8 139.5	VEL 0UT 161.4 168.3 172.2 172.1 172.4 171.9 171.4 1663.1 157.2 152.1	IN 145.1 151.4 154.5		TAN 1N -5.6 -3.7 -0.3 -0.4 3.6 5.9 6.3	VEL OUT -1.5 0.1 2.8 2.1 2.4 2.0 2.0 -1.7 -0.2 2.5	IN 0. 0. 0. 0. 0.	SPEED OUT
RP 1 2 3 4 5 6 7 8 9 10 11	ABS MACH NO IN OUT 0.434 0.484 0.506 0.463 0.518 0.460 0.519 0.458 0.516 0.445 0.502 0.436 0.492 0.436 0.492 0.417 0.456	REL M. 0.454 0.463 0.466 0.460 0.458 0.457 0.445 0.436 0.424 0.417	ACH NO OUT 0.484 0.506 0.518 0.518 0.519 0.518 0.516 0.502 0.490 0.472 0.456	MERID M IN 0.434 0.453 0.463 0.461 0.460 0.458 0.457 0.445 0.445 0.424 0.417	ACH NO OUT 0.484 0.506 0.518 0.518 0.519 0.518 0.516 0.502 0.490 0.472 0.456				PEAK SS MACH NO 0.434 0.454 0.463 0.461 0.460 0.457 0.445 0.436 0.424 0.417

TABLE VII. - Continued.

(c) Reading 867

RP 1 2 3 4 5 6 7 8 9 10 11	RADII IN OUT 25.072 24.971 24.412 24.354 23.058 23.096 21.659 21.806 20.508 20.752 19.334 19.682 18.738 19.139 15.624 16.350 13.960 14.889 12.192 13.365 11.255 12.573	-1.5 0 -1.5 0 -0.4 0 -0.5 0 1.8 0 1.0 0 2.1 -0 2.9 -0 2.4 0	T IN OUT .5 -1.6 -0.5 .1 -1.5 0.1 .9 -1.5 0.9 .6 -0.4 0.6 .8 -0.5 0.8 .7 1.8 0.7 .6 1.0 0.6 .5 2.1 -0.5	IN RATIO 289.0 1.003 288.6 1.003 288.5 1.003 287.9 1.003 287.7 1.002 287.8 1.002 288.0 1.002	TOTAL PRESS IN RATIO 10.03 0.989 10.14 0.994 10.14 0.995 10.14 0.996 10.14 0.996 10.14 0.996 10.14 0.996 10.14 0.993 10.14 0.988 10.14 0.980
RP 1 2 3 4 5 6 7 8 9 10 11	ABS VEL IN OUT 148.0 165.2 154.4 176.3 156.4 176.1 156.2 176.3 155.7 175.7 155.1 170.0 148.3 166.0 144.4 159.3 142.2 152.9	REL VEL IN OUT 148.0 165.2 157.4 176.1 156.4 176.1 155.7 175.1 175.1 175.1 175.1 175.1 175.2 151.3 166.1 144.4 159.1 152.5	5 154.3 172.3 5 157.3 176.3 1 156.4 176.1 5 156.2 176.3 155.6 175.7 2 155.1 175.2 151.2 170.0 148.1 166.0 144.3 159.3	-4.1 2.6 -1.2 1.7 -1.4 2.5 4.9 2.2 2.8 1.9 5.5 -1.4 7.4 -0.1 5.9 1.7	
RP 1 2 5 4 5 6 7 8 9 10 11	ABS MACH NO IN OUT 0.443 0.496 0.463 0.519 0.472 0.531 0.470 0.531 0.469 0.532 0.468 0.530 0.466 0.528 0.454 0.512 0.445 0.500 0.432 0.478 0.425 0.458	REL MACH NO OUT 0.443 0.496 0.463 0.519 0.472 0.533 0.470 0.53 0.469 0.532 0.466 0.532 0.466 0.512 0.445 0.502 0.432 0.478 0.425 0.458	IN 0UT 0.443 0.496 0.463 0.519 0.472 0.531 0.470 0.531 0.469 0.532 0.467 0.530 0.466 0.528 0.466 0.528 0.444 0.512 0.444 0.500 0.432 0.478		MERID PEAK SS VEL R MACH NO 1.117 0.443 1.117 0.463 1.121 0.472 1.126 0.470 1.129 0.468 1.129 0.468 1.124 0.454 1.121 0.445 1.104 0.432 1.076 0.425
RP 1 2 3 4 5 6 7 8 9 10		DENCE SS -13.6 -0.4 -13.5 0.1 -13.5 0.6 -12.4 0.6 -12.5 0.6 -10.2 0.7 -11.0 0.6 -9.9 -0.5 -9.2 -0.0 -9.7 0.6	3 -0.107 0. -0.103 0. 3 -0.101 0. 5 -0.118 0. -0.118 0. -0.122 0. 6 -0.127 0. 6 -0.109 0. -0.105 0. -0.096 0.	LOSS COEFF TOT PROF 0.087 0.087 0.044 0.044 0.036 0.036 0.031 0.031 0.029 0.029 0.030 0.030 0.032 0.032 0.052 0.052 0.052 0.052 0.068 0.068 0.098 0.098 0.169 0.169	LOSS PARAM TOT PROF 0.044 0.044 0.022 0.022 0.017 0.017 0.013 0.013 0.012 0.012 0.012 0.012 0.012 0.012 0.012 0.017 0.017 0.017 0.020 0.020 0.025 0.025 0.040 0.040

TABLE VII. - Continued.

(d) Reading 884

RP 1 2 3 4 5 6 7 8 9 10 11		DUT IN 971 -1.5 354 -1.4 096 -0.9 806 -0.1 752 -0.3 682 -0.0 139 0.2 350 2.6 365 2.0	BETAM OUT -0.6 -0.0 0.5 0.7 0.8 -0.1 0.4	IN -1.5 -1.4 -0.9 -0.1 -0.3 -0.0 0.2 2.3 2.6 2.0	BETAM OUT -0.6 -0.0 0.5 0.7 0.8 -0.1 0.1	TOTAL IN 289.1 288.6 288.1 288.0 287.9 287.9 287.6 287.7 287.9 288.4	TEMP RAT10 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.003 1.002 1.002	TOTAL IN 10.02 10.14 10.14 10.14 10.14 10.15 10.14	PRESS RATIO 0.990 0.994 0.996 0.996 0.995 0.995 0.995 0.985 0.981
RP 1 2 5 4 5 6 7 8 9 10 11	151.6 17 158.5 17 161.8 18 160.8 18 160.7 18 159.8 18 159.1 17 154.9 17 151.8 17	CL REL 1007 IN 100.4 151.6 17.3 158.5 11.5 161.8 11.2 160.8 11.2 160.7 10.5 159.8 19.9 159.1 14.5 154.9 10.1 151.8 13.5 147.7 18.6 145.1	VEL 0UT 170.4 177.3 181.2 181.2 180.5 179.9 174.5 1763.5 158.6	IN 151.5 158.4 161.8 160.8 160.7 159.8 159.1 154.7 151.7	0 VEL 0UT 170.4 177.3 181.5 181.2 181.1 180.5 179.9 174.5 170.1 163.5 158.6	TAN(IN -4.0 -3.8 -2.6 -0.3 -0.9 -0.1 0.5 6.2 6.9 5.5	VEL OUT -1.6 -0.1 2.0 1.5 2.3 2.6 2.4 -0.3 0.4 1.1 2.0	WHEEL IN 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	SPEED OUT 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
RP		UT IN	ACH NO	MERID M IN 0.454	ACH NO OUT 0.512	. ".		VEL R	PEAK SS MACH NO
1 2 3 4 5 6 7 8 9 10	0.476 0. 0.486 0. 0.483 0. 0.481 0. 0.479 0. 0.456 0. 0.456 0.	512 0.454 534 0.476 548 0.486 547 0.483 545 0.483 545 0.479 527 0.465 513 0.456 492 0.442 476 0.434	0.512 0.534 0.548 0.547 0.547 0.545 0.543 0.527 0.513 0.492 0.476	0.475 0.486 0.484 0.483 0.481 0.479 0.465 0.455 0.442	0.534 0.547 0.547 0.547 0.545 0.527 0.513 0.492 0.476			1.125 1.119 1.122 1.127 1.127 1.129 1.129 1.128 1.128 1.108	0.454 0.476 0.486 0.484 0.483 0.481 0.479 0.465 0.456 0.454

TABLE VII. - Concluded.

(e) Reading 895

RP 1 2 3 4 5 6 7 8 9 10		OUT 24.971 24.354 23.096 21.806 20.752 19.682 19.139 16.350 14.889 13.365 12.573	IN -1.8 -1.8 -0.9 0.1 0.2 0.0 1.2 2.5 2.6 3.0 1.7	0UT -0.5 -0.3 0.4 0.6 0.7 0.8	IN -1.8 -1.8 -1.8 -0.9 0.1 0.2 0.0 1.2 2.5 2.6 3.0 1.7	OUT -0.5 -0.3 0.4 0.6 0.7 0.8 -0.3 0.5 0.7 0.6	IN 289.0 288.8 288.3 287.9 287.9 287.9 287.8 287.8 288.0 288.5	RAT10 1.003 1.003 1.004 1.003 1.003 1.003 1.003 1.003 1.002 1.002	IN 10.03 10.14 10.14 10.14 10.14 10.14 10.14	. SPEE
RP 1 23 4 5 6 7 8 9 0 1 1	1N 154.9 161.4 163.2 162.4 161.9 157.8 154.6 152.6 148.1	0UT 174.4 181.2 185.1 185.0 184.9 184.1 163.6 178.1 173.4 166.0 160.4	1N 154.9 161.4 164.3 163.4 163.4 161.9 157.8 154.6 150.1	0UT 174.4 181.2 185.1 185.0 184.9 184.1 183.6 178.1 173.4 166.0	1N 154.9 161.3 164.3 163.4 163.2 162.4 161.9 157.7 154.4 150.3 148.1	0UT 174,4 181,2 185,1 185,0 184,9 184,0 183,5 178,1 173,4 165,9 160,4	N 0 1 5 4 7 1 5 8 1 9 3	OUT -1.6 -0.8 1.0 1.2 1.9 2.7 -1.6 2.1	0. 0. 0. 0. 0.	OUT 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
RP 1 25 4 5 67 8 9 10 11	ABS M IN 0.485 0.495 0.491 0.491 0.487 0.487 0.461 0.454	ACH NO 0.525 0.5240 0.5660 0.5557 0.5558 0.5558 0.5538 0.4482	REL M 1N 0.464 0.485 0.494 0.492 0.491 0.489 0.487 0.464 0.451 0.444	ACH NO OUT 0.525 0.547 0.560 0.560 0.555 0.555 0.555 0.523 0.482	MERID N 1N 0.464 0.484 0.492 0.491 0.487 0.487 0.461 0.451 0.443	MACH NO OUT 0.525 0.5547 0.5559 0.5557 0.5555 0.5558 0.5558 0.482			MERID VEL R 1.126 1.124 1.133 1.133 1.133 1.134 1.130 1.123 1.1083	
RP 1 2 3 4 5 6	PERCENT SPAN 5.00 10.00 20.00 30.00 38.00	MEAN -1.8	DENCE SS -13.8 -13.8 -12.9 -11.9	DEV -0.5 -0.3 0.3 0.4 0.6	D-FACT -0.115 -0.110 -0.117 -0.130 -0.130	EFF 0. 0. 0. 0.	LOSS C TOT 0.078 0.042 0.031 0.025 0.028	0EFF PROF 0.078 0.042 0.031 0.025 0.028	LOSS F TOT 0.039 0.021 0.014 0.011	PARAM PROF 0.039 0.02 0.014 0.015

TABLE VIII. - BLADE-ELEMENT DATA AT BLADE EDGES FOR ROTOR 1

(a) Reading 845

5 186.0 211.9 394.2 256.1 185.9 153.4 2.6 146.2 350.2 3 6 185.3 207.8 379.8 246.0 185.2 151.4 2.3 142.4 333.8 3 7 184.7 209.1 372.2 243.7 184.7 155.0 2.0 140.3 325.1 3 8 179.2 224.5 335.5 218.6 179.2 167.0 -0.9 150.1 282.7 3 9 175.4 222.4 313.2 198.3 175.4 159.7 0.8 154.7 260.2 3 10 170.2 220.1 289.9 186.0 170.2 157.4 2.0 155.9 256.7 3 11 165.4 247.5 276.6 173.9 165.4 163.8 3.3 185.6 225.0 3 ABS NACH NO REL MACH NO MERID MACH NO NERID MACH NO NE	RP 1 2 3 4 5 6 7 8 9 10 11 RP 1 2 3 4	24.795 24.6 24.216 24.0 23.040 22.9 21.841 21.8 20.866 20.9 19.878 20.0 19.378 19.5 16.812 17.3 15.471 16.1 14.079 15.0 13.360 14.4	092	OUT IN 61.9 67.8 51.2 66.2 44.6 64.0 42.2 63.0 43.5 60.8 42.2 61.9 57.7 44.1 55.9 44.4 54.1 48.6 53.3	BETAM OUT 72.2 64.9 59.2 56.5 53.2 52.0 50.5 40.2 36.3 32.2 19.6 ID VEL OUT 83.0 119.9 143.2 151.8	TOTAL TELL IN RAT 289.7 1.2. 289.6 1.2 289.6 1.1 288.7 1.1 288.7 1.1 288.6 1.1 288.3 1.1 288.2 1.1 288.8 1.1 288.8 1.1 388.8 1	IN 22 9.93 10.08 10.08 10.09 10.10 10.10 10.10 10.10 10.07 10.10 10.07 10.02 WHEEL IN 3 415.7 407.6 382.3
7	561-89111 RP1	186.0 211 185.3 207 184.7 209 179.2 224 175.4 222 176.2 220 165.4 247 ABS MACH IN 0U 0.511 0.4 0.558 0.5	1.9 394.2 25 7.8 379.8 24 9.1 372.2 24 4.5 335.5 21 2.4 313.2 19 0.1 289.9 18 7.5 276.6 17 NO REL MACHUT IN CO 478 1.354 0.5 525 1.340 0.5 559 1.275 0.5	66.1 185.9 186.0 185.2 135.7 184.7 18.6 179.2 188.3 175.4 166.0 170.2 135.9 165.4 1 NO MERID NOUT IN 1755 0.511 1776 0.540 777 0.558	153.4 151.4 155.0 167.0 159.7 157.4 163.8 MACH NO OUT 0.225 0.329 0.398	2.6 146 2.3 142 2.0 140 -0.9 150 0.8 154 2.0 153	.2 350.2 .4 333.8 .3 325.1 .1 282.7 .2 260.2 .9 236.7 .6 225.0 MERID 1 VEL R 1 0.489 0.669 0.775
	8 9 10 11	0.565 0.5 0.561 0.5 0.559 0.5 0.542 0.6 0.530 0.6 0.513 0.6 0.497 0.7 PERCENT SPAN M 5.00 10.00	594 1.193 0. 585 1.149 0. 591 1.126 0. 540 1.014 0. 535 0.946 0. 535 0.874 0. 710 0.832 0. INCIDENCE MEAN SS 6.2 3.3 1 5.6 2.4	718 0.563 693 0.561 688 0.559 623 0.542 566 0.530 534 0.513 499 0.497 DEV D-FACT 4.2 0.520	0.430 0.426 0.438 0.476 0.456 0.452 0.470 EFF	TOT PROF 0.341 0.25 0.266 0.18	0.825 0.817 0.839 0.932 0.911 0.925 0.991 LOSS PATOT TOT 0.037 0.039

TABLE VIII. - Continued.

(b) Reading 856

RP 1 2 3 4 5 6 7 8 9 10 11	RADII IN 0UT 24.795 24.656 24.216 24.092 23.040 22.962 21.841 21.831 20.866 20.927 19.878 20.023 19.378 19.571 16.812 17.310 15.471 16.180 14.079 15.049 13.360 14.483	ABS BETAM IN OUT -0.5 61.5 0.0 49.0 0.8 43.2 0.6 41.5 0.7 43.2 0.6 41.3 -0.5 39.7 -0.0 42.6 0.8 46.7	65.6 64.5 63.6 59.6 62.3 56.8 61.2 53.4 60.1 52.4 59.6 50.6 57.0 39.1 55.3 34.1 53.3 30.7	TOTAL TEMP IN RATIO 289.9 1.214 289.6 1.200 289.4 1.178 289.0 1.168 288.8 1.172 288.7 1.160 288.6 1.154 288.3 1.149 288.3 1.146 288.4 1.132 288.8 1.151	TOTAL PRESS IN RATIO 9.93 1.534 10.08 1.584 10.09 1.592 10.10 1.623 10.10 1.564 10.10 1.578 10.08 1.588 10.07 1.578 10.04 1.511 9.99 1.590
R123456789011	ABS VEL IN OUT 176.2 169.4 185.0 190.4 190.8 200.1 191.3 203.1 191.7 211.2 191.0 206.6 190.4 229.9 180.6 232.0 174.5 227.4 169.4 250.9	REL VEL IN OUT 454.5 278.2 447.5 290.0 429.2 288.6 412.1 277.6 397.8 258.2 385.5 249.0 375.6 247.5 338.8 227.9 317.0 207.7 292.2 194.8 279.1 182.4	MERID VEL 1N OUT 176.2 80.8 185.0 124.9 190.8 145.9 191.3 152.1 191.7 153.9 191.0 152.1 190.3 157.2 184.7 157.8 180.6 171.9 174.5 167.5 169.4 172.0	TANG VEL IN OUT -1.5 148.9 0.1 143.7 2.8 136.9 2.1 134.7 2.4 144.6 2.0 139.8 2.0 137.9 -1.6 147.0 -0.2 155.8 2.4 153.7 2.5 182.6	WHEEL SPEED IN OUT 417.5 415.1 407.5 405.4 387.3 386.0 367.1 367.0 350.9 351.9 334.5 337.0 325.8 329.0 282.5 290.8 260.4 272.3 236.8 253.1 224.3 243.2
RP 12334567891011	ABS MACH NO IN OUT 0.531 0.460 0.559 0.523 0.578 0.557 0.580 0.569 0.581 0.592 0.579 0.582 0.577 0.591 0.559 0.657 0.546 0.664 0.527 0.654 0.510 0.721	REL MACH NO IN OUT 1.368 0.755 1.352 0.797 1.300 0.804 1.249 0.778 1.206 0.724 1.163 0.702 1.139 0.700 1.026 0.651 0.959 0.595 0.882 0.560 0.840 0.524	MERID MACH NO IN OUT 0.531 0.219 0.559 0.343 0.578 0.406 0.580 0.426 0.581 0.432 0.579 0.428 0.577 0.444 0.559 0.505 0.546 0.492 0.527 0.482 0.510 0.495		MERID PEAK SS VEL R MACH NO 0.458 1.568 0.675 1.536 0.765 1.495 0.795 1.483 0.803 1.470 0.796 1.464 0.826 1.464 0.957 1.474 0.951 1.436 0.960 1.345 1.016 1.300
RP 1 2 3 4 5 6 7 8 9 10	PERCENT INC SPAN MEAN 5.00 5.6 10.00 5.0 20.00 5.0 30.00 5.7 38.00 6.0 46.00 6.5 50.00 6.7 70.00 8.0 80.00 8.3 90.00 8.6	IDENCE DEV SS 2.7 15.2 1.8 7.4 1.2 4.4 1.4 3.8 1.4 2.7 1.4 4.3 1.4 4.1 1.9 3.6 1.9 6.5 2.0 13.1 2.4 7.8	D-FACT EFF 0.504 0.608 0.462 0.702 0.429 0.795 0.426 0.847 0.457 0.861 0.453 0.852 0.442 0.902 0.434 0.947 0.456 0.951 0.441 0.946 0.474 0.936	LOSS COEFF TOT PROF 0.327 0.237 0.244 0.164 0.163 0.098 0.122 0.067 0.119 0.072 0.124 0.083 0.082 0.045 0.051 0.024 0.051 0.035 0.058 0.054 0.083 0.082	LOSS PARAM TOT PROF 0.033 0.024 0.036 0.024 0.027 0.016 0.021 0.011 0.021 0.013 0.021 0.014 0.014 0.008 0.009 0.004 0.009 0.004 0.009 0.009 0.015 0.015

TABLE VIII. - Continued.

(c) Reading 867

RP 1 2 3 4 4 5 6 7 8 9 10	RP 1 23 4 5 6 7 8 9 10 11	RP 1 233 4 5 6 7 8 9 0 1 1	RP 1 2 3 4 5 6 7 8 9 10 11
PERCENT SPAN 5.00 10.00 20.00 30.00 38.00 46.00 50.00 70.00 80.00	ABS M 1N 0.545 0.575 0.594 0.596 0.597 0.595 0.572 0.572 0.535 0.513	ABS IN 180.7 189.8 196.3 196.7 195.8 195.0 188.5 184.1	RAD IN . 24.795 24.216 23.040 21.841 20.866 19.878 19.378 16.812 15.471 14.079 13.360
INCI MEAN 5.0 4.3 5.0 5.3 5.8 6.0 7.4 7.6	ACH NO OUT 0.436 0.516 0.556 0.568 0.575 0.575 0.570 0.670 0.682 0.674 0.725	VEL 0UT 160.0 186.6 198.7 202.3 209.3 203.9 203.9 237.5 233.8 251.9	0UT 24.656 24.092 22.962 21.831 20.927 20.023 19.571 17.310 16.180 15.049
DENCE SS 2.1 1.1 0.6 0.7 0.6 0.7 1.3	REL M 1.371 1.357 1.357 1.256 1.211 1.170 1.145 1.033 0.961 0.887 0.845	REL IN 454.8 448.4 430.7 398.6 385.1 377.0 340.6 317.5 293.9 280.7	IN -0.4 0.1 0.8 0.5 0.7
DEV 16.2 7.2 4.2 3.7 2.8 4.7 4.1 3.0 5.2	ACH NO 0.776 0.835 0.836 0.795 0.712 0.715 0.677 0.618 0.584 0.544	VEL 0UT 284.9 302.0 298.7 282.9 260.1 252.1 252.2 236.3 215.3 202.6 188.9	BETAM OUT 60.9 45.2 40.1 39.8 42.4 41.6 39.7 37.8 40.4 40.9 45.1
D-FACT 0.482 0.427 0.401 0.412 0.451 0.444 0.428 0.410 0.431	MERID M IN 0.545 0.575 0.594 0.596 0.597 0.595 0.572 0.572 0.535 0.513	MERI IN 180.7 189.8 195.9 196.6 195.8 195.0 188.5 184.1 177.1	RELLIN 66.6 65.0 63.0 61.7 60.4 59.4 58.9 56.4 54.6 52.9
EFF 0.597 0.727 0.805 0.844 0.840 0.827 0.892 0.947	ACH NO OUT 0.212 0.364 0.426 0.437 0.434 0.430 0.454 0.530 0.520 0.509 0.512	D VEL OUT 77.9 131.4 155.5 154.6 152.4 160.1 184.7 181.0 176.6	BETAM 0UT 74.1 64.2 59.4 56.7 53.5 52.8 50.6 38.6 32.8 29.3 19.9
LOSS C TOT 0.318 0.209 0.145 0.119 0.132 0.139 0.087 0.049 0.052		IN -1.3 0.3 2.6 1.7 2.5 2.2	TOTA IN 289.9 289.6 289.4 289.0 288.7 288.7 288.4 288.4 288.5 288.8
0EFF PROF 0.231 0.131 0.083 0.066 0.100 0.052 0.024 0.038		G VEL OUT 139.7 132.5 127.9 129.3 141.1 135.4 132.9 143.4 153.8 153.2	L TEMP RATIO 1.200 1.183 1.166 1.161 1.168 1.154 1.148 1.145 1.144 1.132
LOSS F TOT 0.031 0.024 0.020 0.023 0.024 0.015 0.009		WHEEL IN 416.1 406.5 386.3 365.8 349.2 333.8 324.5 282.3 258.6 236.2 223.9	TOTAL IN 9.92 10.08 10.09 10.10 10.10 10.10 10.07 10.05 10.02 9.94
PARAM PROF 0.022 0.020 0.014 0.011 0.015 0.017 0.009 0.004 0.007	PEAK SS MACH NO 1.551 1.519 1.479 1.466 1.449 1.446 1.440 1.457 1.417 1.342 1.308	SPEED OUT 413.7 404.4 385.0 365.7 350.2 327.7 290.7 270.5 252.4 242.8	PRESS RATIC 1.484 1.550 1.550 1.561 1.586 1.522 1.544 1.568 1.565 1.509

TABLE VIII. - Continued.

(d) Reading 884

RP 1 2 3 4 5 6 7 8 9 10 11	RADII IN OUT 24.795 24.656 24.216 24.092 23.040 22.962 21.841 21.831 20.866 20.927 19.878 20.023 19.378 19.571 16.812 17.310 15.471 16.180 14.079 15.049 13.360 14.483	ABS BETAM IN OUT -0.5 59. -0.0 41. 0.6 35. 0.4 36. 0.6 40. 0.7 40. 0.7 38. -0.1 35. 0.1 37. 0.3 39. 0.6 43.	IN 0UT 6 65.9 75.4 1 64.4 63.5 5 62.4 58.9 6 61.1 56.2 4 59.9 53.6 2 58.8 53.7 4 58.2 51.1 5 55.6 38.9 2 54.0 33.8 3 52.3 27.6	TOTAL TEMP IN RATIO 289.9 1.184 289.7 1.172 289.4 1.152 289.0 1.153 288.9 1.162 288.8 1.147 288.7 1.144 288.4 1.38 288.3 1.36 288.4 1.34 288.7 1.147	TOTAL PRESS IN RATIO 9.92 1.415 10.07 1.516 10.10 1.528 10.10 1.547 10.10 1.457 10.09 1.491 10.06 1.536 10.04 1.531 9.99 1.532 9.95 1.552
RP 1 2 3 4 5 6 7 8 9 10 11	ABS VEL IN OUT 186.8 148.1 195.9 187.2 202.3 200.6 202.7 204.9 202.7 209.8 201.7 200.2 200.9 207.1 194.1 235.7 189.1 239.8 182.1 244.1 177.2 254.9	REL VEL IN OUT 458.3 296.3 452.8 316.1 436.0 315.9 269.4 388.9 258.4 381.5 258.5 343.8 246.6 322.0 229.9 298.1 213.3 285.2 195.8	195.9 141.0 202.3 163.3 202.7 164.6 202.7 159.8 201.7 152.9 200.9 162.2 194.1 191.9 189.1 191.0 182.1 188.9	TANG VEL IN OUT -1.7 127.8 -0.1 123.1 2.0 116.5 1.5 122.1 2.3 135.9 2.6 129.2 2.4 128.7 -0.3 136.8 0.3 144.9 1.0 154.5 1.8 176.6	WHEEL SPEED IN OUT 416.8 414.5 408.2 486.9 368.5 368.4 351.7 352.7 335.0 337.5 326.7 330.0 283.4 291.8 261.0 272.9 237.1 253.4 225.3 244.2
RP 1 2 3 4 5 6 7 8 9 10	ABS MACH NO IN OUT 0.564 0.405 0.594 0.520 0.615 0.565 0.617 0.579 0.617 0.566 0.611 0.588 0.590 0.678 0.574 0.692 0.551 0.736	REL MACH NO IN OUT 1.385 0.811 1.373 0.879 1.326 0.890 1.276 0.837 1.230 0.759 1.184 0.731 1.161 0.734 1.044 0.710 0.977 0.661 0.965	IN OUT 0.564 0.205 0.594 0.392 0.615 0.460 0.617 0.465 0.617 0.450 0.614 0.432 0.611 0.461 0.590 0.552 0.574 0.551 0.551 0.547		MERID PEAK SS VEL R MACH NO 0.401 1.542 0.720 1.515 0.807 1.477 0.812 -1.465 0.789 1.446 0.758 1.434 0.808 1.435 1.010 1.422 1.037 1.345 1.037 1.301
RP 1 2 3 4 5 6 7 8 9 10 11	PERCENT INC SPAN MEAN 5.00 4.3 10.00 3.8 20.00 3.7 30.00 4.4 38.00 4.7 46.00 5.1 50.00 5.4 70.00 6.7 80.00 7.1 90.00 7.6	IDENCE SS 1.4 17.4 0.6 6.5 -0.0 3.7 0.2 3.3 0.1 2.9 0.1 5.7 0.6 3.4 0.7 6.2 1.0 10.1 1.3 8.6	0.452 0.565 0.395 0.734 0.361 0.820 0.383 0.843 0.431 0.818 0.428 0.770 0.414 0.841	LOSS COEFF TOT PROF 0.318 0.231 0.192 0.112 0.124 0.059 0.113 0.058 0.143 0.097 0.173 0.135 0.125 0.087 0.048 0.024 0.047 0.031 0.037 0.033 0.111 0.109	LOSS PARAM TOT PROF 0.028 0.020 0.029 0.017 0.021 0.010 0.020 0.010 0.025 0.017 0.029 0.023 0.021 0.015 0.009 0.005 0.009 0.006 0.007 0.006 0.020 0.019

TABLE VIII. - Concluded.

(e) Reading 895

RP 1 2 3 4 5 6 7 8 9 10 11	RAD IN 24.795 24.216 23.040 21.841 20.866 19.878 19.378 16.812 15.471 14.079 13.360	0UT 24.656 24.092 22.962 21.831 20.927 20.023 19.571 17.310 16.180 15.049	ABS IN -0.5 -0.2 0.3 0.5 0.6 0.7 -0.3 0.5 0.6	BETAM OUT 44.4 33.6 30.7 31.7 36.0 36.8 33.7 34.4 37.3 40.7	RELL IN 65.5 63.9 61.9 60.5 59.3 58.2 57.6 55.1 53.3 51.9	BETAM OUT 69.2 63.7 59.9 57.1 55.5 57.0 54.0 38.7 33.4 25.9 20.6	1N 289.9 289.7 289.3 -289.0 288.9 288.8 288.8 288.5	L TEMP RAT10 1.163 1.142 1.131 1.132 1.141 1.126 1.135 1.130 1.134	TOTAL IN 9.92 10.08 10.09 10.10 10.09 10.09 10.05 9.97 9.91	PRESS RATIO 1.364 1.414 1.433 1.438 1.458 1.334 1.376 1.488 1.503 1.535 1.535
RP 1 2 3 4 5 6 7 8 9 0 1 1	ABS 191.6 200.6 206.9 207.5 207.4 206.2 205.5 198.6 193.2 185.2	VEL 0UT 161.2 181.7 194.4 199.9 200.0 184.2 239.3 246.2 246.1 261.0	REL IN 461.8 456.2 439.5 421.7 406.8 391.9 383.8 347.3 323.5 299.8 286.9	VEL 0UT 324.7 341.5 333.0 313.1 285.5 271.1 267.7 255.2 243.4 211.4	MERI IN 191.6 200.6 206.9 207.5 207.4 206.2 205.5 198.6 193.2 185.1	D VEL 0UT 115.2 151.3 167.1 170.0 161.7 147.5 157.4 199.1 203.2 203.6 198.0	IN -1.6 -0.8 1.0 1.2 1.9 2.2 2.6 -1.5 2.5	G VEL OUT 112.7 100.7 99.3 105.1 117.7 110.3 113.6 132.8 139.0 155.3	WHEEL 18.6 418.6 408.9 388.7 368.3 351.9 335.4 326.8 284.0 261.0 237.8 225.4	SPEED 0UT 416.2 406.8 387.4 368.1 352.9 337.8 330.1 292.4 272.9 254.2 244.4
RP 1 2 5 4 5 6 7 8 9 10 11	ABS M IN 0.580 0.630 0.633 0.633 0.633 0.629 0.626 0.687 0.542	ACH NO 0.447 0.551 0.552 0.569 0.567 0.523 0.553 0.690 0.714 0.757	REL M 1.398 1.386 1.339 1.286 1.241 1.195 1.170 1.056 0.982 0.908 0.866	ACH NO 0UT 0.900 0.961 0.946 0.891 0.809 0.770 0.763 0.763 0.736 0.658 0.613	MERID M IN 0.580 0.609 0.633 0.633 0.633 0.629 0.626 0.604 0.587 0.561	ACH NO OUT 0.319 0.426 0.475 0.184 0.459 0.419 0.574		•		PEAK SS MACH NO 1.539 1.512 1.475 1.454 1.437 1.426 1.418 1.424 1.406 1.339 1.302
RP 1 2 3 4 5 6 7 8 9 10	PERCENT SPAN 5.00 10.00 20.00 30.00 38.00 46.00 50.00 70.00	INCE MEAN 3.9 3.3 3.8 4.2 4.8 6.4	DENCE SS 1.0 0.1 -0.4 -0.5 -0.5 -0.5	DEV 11.3 6.7 4.7 4.1 4.7 9.0 7.5 3.1 5.8	D-FACT 0.384 0.328 0.315 0.334 0.383 0.383 0.383 0.359 0.344	EFF 0.569 0.734 0.826 0.829 0.808 0.608 0.755 0.893 0.953	LOSS C TOT 0.284 0.162 0:104 0.108 0.133 0.206 0.165 0.089 0.042	OEFF PROF 0.196 0.081 0.038 0.053 0.087 0.167 0.130 0.066 0.028	LOSS P TOT 0.035 0.025 0.017 0.018 0.022 0.032 0.032 0.017 0.018	PROF 0.024 0.012 0.006 0.009 0.015 0.026 0.021 0.012 0.012

TABLE IX. - BLADE-ELEMENT DATA AT BLADE EDGES FOR STATOR 1

(a) Reading 845

RP 1 2 3 4 5 6 7 8 9 10 11	RADII IN OUT 24.447 24.359 23.937 23.896 22.913 22.969 21.887 22.037 21.064 21.290 20.239 20.544 19.827 20.173 17.767 18.326 16.739 17.412 15.715 16.500 15.207 16.040	ABS BETAM IN OUT 59.3 1.8 48.1 2.9 41.2 1.7 38.9 -0.5 40.3 1.1 40.0 -0.7 38.8 -0.8 38.4 0.8 40.5 -0.9 40.5 -2.2 44.7 -1.2	48.1 2.9 41.2 1.7 38.9 -0.5 40.3 1.1 40.0 -0.7 38.8 -0.8 38.4 0.8 40.5 -0.9 40.5 -2.2	TOTAL TEMP IN RATIO 354.2 0.989 349.3 0.996 342.2 0.997 338.1 0.998 338.9 0.992 335.5 0.997 331.9 0.994 329.8 0.997 326.5 1.011 332.9 0.996	TOTAL PRESS IN RATIO 15.47 1.019 16.01 1.000 16.18 0.991 16.25 0.986 16.51 0.964 16.00 0.965 16.05 0.959 16.11 0.965 15.76 0.976 15.20 1.014 16.06 0.942
RP 1 2 3 4 5 6 7 8 9 5 1 1	ABS VEL IN OUT 182.2 171.1 201.9 176.6 -214.3 180.4 218.6 179.3 224.6 173.6 219.4 163.9 220.9 160.7 235.5 154.8 230.4 153.4 226.7 146.3 251.3 136.7	REL VEL 1N OUT 182.2 171.1 201.9 176.6 214.3 180.4 218.6 179.3 224.6 173.6 219.4 163.9 220.9 160.7 235.5 154.8 230.4 153.4 226.7 146.3 251.3 136.7	MERID VEL IN OUT 93.1 171.0 134.9 176.4 161.1 180.3 170.2 179.3 171.3 173.6 168.1 163.9 172.1 160.7 184.6 154.8 175.3 153.4 172.3 146.2 178.6 136.6	TANG VEL IN OUT 156.6 5.2 150.3 8.9 141.3 5.4 137.1 -1.6 145.2 3.5 140.9 -2.1 138.5 -2.1 146.2 2.1 149.5 -2.5 147.4 -5.5 176.8 -2.9	WHEEL SPEED IN OUT 0.
RP 1 2 3 4 5 6 7 8 9 11 1	ABS MACH NO IN OUT 0.495 0.466 0.555 0.483 0.598 0.499 0.615 0.499 0.633 0.483 0.620 0.456 0.627 0.448 0.674 0.433 0.660 0.430 0.652 0.408 0.722 0.380	REL MACH NO IN OUT 0.495 0.466 0.555 0.483 0.598 0.499 0.615 0.483 0.620 0.456 0.627 0.448 0.674 0.433 0.660 0.430 0.652 0.380	MERID MACH NO IN OUT 0.253 0.466 0.371 0.483 0.450 0.499 0.479 0.499 0.482 0.483 0.475 0.456 0.488 0.448 0.528 0.433 0.502 0.430 0.496 0.438		MERID PEAK SS VEL R MACH NO 1.837 1.149 1.308 1.054 1.119 0.990 1.054 0.959 1.014 1.006 0.975 0.966 0.934 0.944 0.838 0.954 0.875 0.950 0.849 0.905 0.765 1.084
RP 1 2 3 4 5 6 7 8 9 10 11	PERCENT INCI SPAN MEAN 5.00 24.0 10.00 13.1 20.00 7.0 30.00 4.8 38.00 5.7 46.00 4.6 50.00 3.0 70.00 -0.1 80.00 0.2 90.00 -1.8 95.00 1.4	DENCE DEV SS 17.2 10.2 6.6 11.2 0.8 9.6 -1.0 7.1 0.2 8.7 -0.5 6.9 -1.9 6.9 -4.3 8.5 -3.7 6.9 -5.4 5.9 -2.0 6.9	D-FACT EFF 0.334 0. 0.351 0. 0.354 0. 0.366 0. 0.405 0. 0.442 0. 0.442 0. 0.481 0. 0.494 0. 0.599 0.	LOSS COEFF TOT PROF -0.126 -0.126 0.000 0.000 0.040 0.040 0.060 0.060 0.154 0.154 0.151 0.151 0.176 0.176 0.135 0.135 0.094 0.094 -0.055 -0.055 0.196 0.196	LOSS PARAM TOT PROF -0.041 -0.041 0.000 0.000 0.012 0.012 0.018 0.018 0.044 0.044 0.041 0.041 0.047 0.047 0.032 0.032 0.021 0.021 -0.012 -0.012 0.040 0.040

TABLE IX. - Continued.

(b) Reading 856

RP 1 2 3 4 5 6 7 8 9 10 11	RP 1 2 3 4 5 6 7 8 9 10 11	R 1 2 3 4 5 6 7 8 9 5 1	RP 1 2 3 4 5 6 7 8 9 10 11
PERCENT SPAN 5.00 10.00 20.00 30.00 38.00 46.00 50.00 70.00 80.00 90.00 95.00	IN 0.477	ABS IN 175.3 201.8 211.1 217.1 224.0 218.4 221.4 243.0 242.1 235.8 256.3	RAD IN 24.447 23.937 21.887 21.064 20.239 19.827 17.767 16.739 15.715
INCI MEAN 23.6 10.8 5.6 4.1 5.3 4.0 -2.4 -1.8 -3.7	ACH NO OUT 0.451 0.485 0.509 0.506 0.487 0.463 0.471 0.468 0.425	VEL 0UT 165.4 176.6 183.1 181.5 174.8 165.5 167.6 166.3 160.2 152.2	0UT 24.359 23.896 22.969 22.037 21.290 20.544 20.173 18.326 17.412 16.500
DENCE SS 16.9 4.3 -0.6 -1.7 -0.2 -1.2 -2.9 -6.6 -5.7 -7.3 -4.0	REL M IN 0.477 0.557 0.599 0.611 0.631 0.618 0.629 0.698 0.696 0.680	REL IN 175.3 201.8 214.1 217.1 224.0 218.4 221.4 243.0 242.1 235.8 256.3	ABS 1N 58.9 45.8 39.9 38.2 39.9 39.3 37.9 36.1 38.5 38.6 42.7
DEV 10.8 11.3 7.7 7.1 8.7 5.7 6.1 8.2 6.8 5.3 6.8	ACH NO 0.451 0.485 0.509 0.506 0.487 0.462 0.463 0.471 0.468 0.449	VEL 0UT 165.4 176.6 183.1 181.5 174.8 165.5 167.6 166.3 160.2	BETAM OUT 2.4 3.0 -0.1 -0.5 1.1 -1.9 -1.5 0.5 -1.0 -2.7
D-FACT 0.325 0.341 0.343 0.348 0.397 0.421 0.421 0.424 0.454 0.457	MERID M 1N 0.246 0.388 0.460 0.480 0.484 0.478 0.496 0.564 0.545 0.531 0.542	MERI IN 90.5 140.8 164.4 170.6 171.9 169.0 174.7 196.3 189.6 184.1	REL 1N 58.9 45.8 39.9 39.2 39.3 37.9 36.1 38.5 38.6 42.7
EFF 0. 0. 0. 0. 0. 0. 0.	ACH NO OUT 0.450 0.509 0.506 0.487 0.462 0.463 0.471 0.468 0.448	D VEL 0UT 165.3 176.4 183.1 181.5 174.7 165.4 165.4 167.6 166.2 160.0	BETAM OUT 2.4 3.0 -0.1 -0.5 1.1 -1.9 -1.5 0.5 -1.0 -2.7
LOSS C TOT -0.118 0.027 0.014 0.039 0.152 0.148 0.162 0.124 -0.034 0.167		TAN IN 150.2 144.6 137.2 134.3 143.6 138.3 143.2 150.6 147.9	TOTA IN 351.9 347.5 340.9 337.4 338.6 334.9 333.1 331.3 330.5 326.6 332.5
PROF -0.118 0.027 0.014 0.039 0.152 0.148 0.162 0.124 0.124		0VEL 0UT 6.9 9.2 -0.4 -1.7 3.3 -5.5 -4.4 1.5 -3.0 -7.6 -3.6	L TEMP RATIO 0.993 0.995 0.997 0.991 0.995 0.997 0.994 1.010 0.997
LOSS f TOT -0.039 0.009 0.004 0.012 0.043 0.040 0.043 0.030 0.028 -0.007		WHEEL IN 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	TOTAL IN 15.23 15.96 16.03 16.06 15.80 15.93 16.00 15.89 15.17
PROF -0.039 0.009 0.004 0.012 0.043 0.040 0.043 0.030 0.028	PEAK SS MACH NO 1.100 1.012 0.962 0.940 0.995 0.928 0.933 0.954 0.898 1.060	SPEED OUT 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	PRESS RATIO 1.017 0.995 0.997 0.991 0.964 0.966 0.962 0.965 0.966 1.009 0.949

TABLE IX. - Continued.

(c) Reading 867

RP 1 2 3 4 5 6 7 8 9 10 11	RADII IN 0U 24.447 24.3 23.937 23.8 22.913 22.9 21.887 22.0 21.064 21.2 20.239 20.5 19.827 20.1 17.767 18.3 16.739 17.4 15.715 16.5 15.207 16.0	T IN 59 58.2 96 41.9 69 36.7 37 36.4 90 39.1 44 38.3 73 36.4 26 34.1 12 36.5 00 37.0	S BETAM OUT 2.4 1.8 -1.0 -0.8 0.9 -2.3 -2.0 -1.0 -1.3 -3.7 -1.9	REL 1N 58.2 41.9 36.7 36.4 39.1 38.3 36.4 34.1 36.5 37.0 41.1	BETAM OUT 2.4 1.8 -1.0 -0.8 0.9 -2.3 -2.0 -1.0 -1.3 -3.7 -1.9	TOTA IN 347.9 342.7 337.4 335.5 337.2 333.2 331.5 330.2 329.9 326.6 331.8	L TEMP RATIO 0.994 0.995 0.997 0.989 0.993 0.995 0.992 1.005	TOTAL IN 14.72 15.62 15.63 15.76 16.01 15.37 15.59 15.80 15.74	PRESS RATIO 1.021 0.990 1.000 0.965 0.965 0.964 0.964 0.966 1.000 0.962
RP 1 23 4 5 6 7 8 9 11	ABS VEL IN 165.7 166 199.5 179 214.3 186 217.2 186 222.4 179 216.0 169 221.3 170 249.0 179 249.6 177 244.0 173 258.8 168	T IN .7 165.7 199.5 .9 214.3 .7 217.2 .222.4 .8 216.0 .2 221.3 .1 249.0 .3 249.6 .4 244.0	VEL 0UT 166.7 179.5 186.9 186.7 179.2 169.8 170.2 179.1 177.3 173.4	MERI 187.2 148.4 171.8 174.7 172.7 169.5 178.2 206.2 206.6 194.9 195.0	D VEL 00T 166.6 179.4 186.8 186.6 179.2 169.7 170.1 179.0 177.2	TAN IN 140.9 133.3 128.1 129.0 140.2 134.0 131.2 139.7 148.6 146.7 170.0	0 VEL 0UT 7.0 5.6 -3.2 -2.6 2.9 -6.8 -5.8 -3.0 -4.0 -11.1 -5.6	WHEEL IN	SPEED OUT 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
RP 1 2 3 4 5 6 7 8 9 10 11	ABS MACH IN 0.452 0.4 0.554 0.4 0.603 0.5 0.613 0.5 0.628 0.5 0.612 0.4 0.630 0.4 0.718 0.5 0.720 0.5 0.747 0.4	T IN 57 0.452 96 0.554 23 0.603 23 0.613 0.628 76 0.612 78 0.630 0.718 0.720 89 0.706	0.457 0.457 0.496 0.523 0.523 0.502 0.476 0.478 0.501 0.489 0.474	MERID M IN 0.238 0.412 0.483 0.493 0.488 0.480 0.507 0.595 0.579 0.564 0.563	0.456 0.456 0.496 0.522 0.523 0.502 0.476 0.478 0.506 0.474				PEAK SS MACH NO 1.032 0.934 0.905 0.906 0.972 0.920 0.896 0.908 0.938 0.888 1.029
RP 1 2 3 4 5 6 7 8 9 10 11	SPAN MI 5.00 2 10.00 20.00 30.00 38.00 46.00 50.00 70.00	INCIDENCE EAN SS 2.9 16.2 7.0 0.4 2.5 -3.7 2.3 -3.4 4.4 -1.0 3.0 -2.1 0.6 -4.4 4.4 -8.6 5.8 -7.6 5.4 -9.0 2.2 -5.7	DEV 10.9 10.1 6.8 8.5 5.6 6.6 4.4 6.2	D-FACT 0.260 0.307 0.317 0.319 0.369 0.391 0.395 0.416 0.425 0.423 0.483	EFF 0. 0. 0. 0. 0. 0. 0.	LOSS COTOT -0.161 0.051 0.001 0.046 0.149 0.141 0.168 0.124 0.117 -0.001 0.123	PROF -0.161 0.051 0.001 0.046 0.149 0.141 0.168 0.124 0.117	LOSS P TOT -0.053 0.016 0.000 0.014 0.038 0.045 0.030 0.027 -0.000 0.025	PROF -0.053 0.016 0.000 0.014 0.042 0.038 0.045 0.030 0.027

TABLE IX. - Continued.

(d) Reading 884

RP123456789011 R1234	RADII IN OUT 24.447 24.359 23.937 23.896 22.913 22.969 21.887 22.037 21.064 21.290 20.239 20.544 19.827 20.173 17.767 18.326 16.739 17.412 15.715 16.500 15.207 16.040 ABS VEL IN OUT 153.7 169.5 202.2 186.4 219.2 196.9	IN 57.0 37.8 32.2 33.2 33.2 35.1 31.8 33.3 35.2 39.7 REL IN 153.7 202.2	0.4 -2.9 -2.0 -2.0 -3.3 -1.6 VEL 0UT 169.5 186.4 195.8 196.9	IN 57.0 37.8 32.2 33.2 37.0 36.9 35.1 31.8 33.3 35.2	D VEL 001 1.96.9 196.9	TOTAL TEMP IN RATIO 343.4 0.992 339.4 0.993 335.7 0.997 335.7 0.997 335.7 0.992 328.2 0.992 327.6 0.993 327.1 0.996 331.2 0.992 TANG VEL IN OUT 128.9 5.3 123.9 2.1 116.7 -7.4 121.8 -3.9	TOTAL PRES IN RATI 14.03 1.02 15.27 0.97 15.24 0.96 15.62 0.96 14.71 0.97 15.04 0.95 15.37 0.97 15.31 0.97 15.31 0.97 15.31 0.97 WHEEL SPEE IN OUT 0. 0. 0. 0.
5 6 7 8 9 10 11 RP	224.2 189.9 212.7 179.0 221.0 179.8 253.2 191.6 255.1 188.8 256.8 187.6 263.2 188.0 ABS MACH NO IN OUT	212.7 221.0 253.2 255.1 256.8 263.2 REL M	189.9 179.0 179.8 191.6 188.8 187.6 188.0	179.0 170.0 180.8 215.3 213.2 209.9 202.4 MERID N	OUT	135.0 1.5 127.8 -9.1 127.0 -8.8 133.3 -6.5 140.1 -6.5 148.0 -10.6 168.2 -5.2	0. 0. 0. 0. 0. 0. 0. 0. 0. 0. MERID PEAK VEL R MACH
1 2 3 4 5 6 7 8 9 10	0.421 0.468 0.565 0.520 0.622 0.556 0.635 0.535 0.604 0.505 0.630 0.508 0.754 0.545 0.741 0.537 0.747 0.533 0.762 0.532	0.565 0.622 0.631 0.635 0.604 0.630 0.734	0.468 0.552 0.552 0.555 0.535 0.505 0.508 0.545 0.537 0.533	0.229 0.446 0.526 0.528 0.507 0.483 0.516 0.624 0.619 0.610	0.468 0.520 0.552 0.555 0.535 0.505 0.508 0.545 0.537 0.532		2.023 0.94 1.167 0.87 1.054 0.86 1.059 0.86 1.061 0.93 1.051 0.87 0.993 0.86 0.889 0.85 0.885 0.87 0.892 0.88
RP 1 2 3 4 5 6 7 8 9	PERCENT IN SPAN MEAN 5.00 21. 10.00 2. 20.00 -0. 38.00 2. 46.00 1. 50.00 -0. 80.00 -7. 90.00 -7. 95.00 -3.	7 14.9 8 -3.7 1 -8.3 9 -6.7 4 -3.0 6 -3.6 7 -5.7 7 -11.0 0 -10.9 2 -10.7	DEV 10.2 8.9 5.7 6.5 8.0 4.7 4.8 5.9 4.8 6.5	D-FACT 0.161 0.272 0.282 0.280 0.322 0.353 0.355 0.374 0.387 0.398 0.418	EFF 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	LOSS COEFF TOT PROF -0.208 -0.208 0.119 0.119 0.053 0.053 0.073 0.073 0.168 0.168 0.115 0.115 0.176 0.176 0.091 0.091 0.083 0.083 0.073 0.073 0.090 0.090	LOSS PARAM TOT PROF -0.068 -0.06 0.038 0.03 0.016 0.01 0.022 0.02 0.048 0.04 0.031 0.03 0.047 0.04 0.022 0.02 0.019 0.01 0.015 0.019

TABLE IX. - Concluded.

(e) Reading 895

RP 1 2 3 4 5 6 7 8 9 10	RAD IN 24.447 23.937 22.913 21.887 21.064 20.239 19.827 17.767 16.739 15.715 15.207	OUT 24.359 23.896 22.969 22.037 21.290 20.544 20.173 18.326 17.412 16.500	ABS (N 41.1 30.5 27.6 28.6 32.8 33.7 32.6 29.9 30.4 33.0 36.3	BETAM OUT 0.0 -1.4 -3.3 -2.7 -1.0 -3.9 -4.3 -3.0 -3.3 -2.4 0.1	REL (N 41.1 30.5 27.6 28.6 32.8 33.7 32.6 29.9 30.4 33.0 36.3	BETAM OUT 0.0 -1.4 -3.3 -2.7 -1.0 -3.9 -4.3 -3.0 -3.3 -2.4 0.1	TOTA IN 337.2 330.8 327.3 327.1 329.6 325.2 325.3 327.4 325.8 327.2 329.8	RAT10 0.987 0.996 0.996 0.997 0.989 0.993 0.990 0.988 0.989	TOTAL IN 13.53 14.25 14.46 14.53 14.72 13.47 13.88 14.97 15.08 15.30	PRESS RATIO 0.983 0.980 0.968 0.965 0.951 0.959 0.957 0.958 0.955
RP 1 2 3 4 5 6 7 8 9 10 11	ABS IN 172.7 199.9 214.8 219.3 215.9 196.9 208.1 259.3 265.7 272.8 273.5	VEL 0UT 184.7 203.6 211.0 211.6 207.2 196.0 195.2 209.3 213.8 217.8	REL IN 172.7 199.9 214.8 219.3 215.9 196.9 208.1 259.3 265.7 272.8 273.5	VEL 0UT 184.7 203.6 211.0 211.6 207.2 196.0 195.2 209.3 217.8	MERI 172.3 190.3 192.6 181.4 163.8 175.2 224.8 229.3 228.7 220.3	D VEL 0UT 184.7 203.6 210.7 211.4 207.2 195.5 194.7 209.1 213.7 217.8	IN 113.6 101.3 99.5 104.9 116.9 112.2 112.3 134.3 148.7 162.0	OUT 0.1 -5.0 -12.0 -10.1 -3.6 -13.5 -14.5 -12.2 -8.9 0.3	WHEEL IN 0. 0. 0. 0. 0. 0.	SPEED OUT 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
RP 1 2 5 4 5 6 7 8 9 10 11	ABS M IN 0.480 0.566 0.614 0.628 0.615 0.562 0.755 0.778 0.799 0.798	ACH NO 0UT 0.519 0.578 0.604 0.606 0.592 0.561 0.559 0.609 0.616 0.625	REL M IN 0.480 0.566 0.614 0.628 0.562 0.562 0.755 0.778 0.799 0.798	ACH NO OUT 0.519 0.578 0.604 0.606 0.592 0.561 0.569 0.609 0.616 0.625	MERID M IN 0.361 0.488 0.544 0.552 0.517 0.467 0.654 0.671 0.670 0.643	ACH NO OUT 0.519 0.578 0.603 0.605 0.592 0.560 0.558 0.601 0.608 0.615 0.625				PEAK SS MACH NO 0.798 0.730 0.718 0.749 0.820 0.753 0.768 0.817 0.786 0.868 0.958
RP 1 2 3 4 5 6 7 8 9 10	PERCENT SPAN 5.00 10.00 20.00 30.00 38.00 46.00 50.00 70.00 80.00	INCI MEAN 5.9 -4.5 -6.6 -5.6 -1.7 -3.6 -9.9	DENCE 5S -0.9 -11.1 -12.8 -11.3 -7.3 -6.8 -8.2 -12.8 -13.8	DEV 8.5 6.8 4.6 4.9 6.6 3.7 3.3 4.7	D-FACT 0.147 0.153 0.178 0.190 0.198 0.174 0.224 0.321 0.327	EFF 0. 0. 0. 0. 0. 0.	LOSS C TOT 0.115 0.105 0.143 0.149 0.217 0.071 0.137 0.128	OEFF PROF 0.115 0.105 0.143 0.149 0.217 0.071 0.194 0.137 0.128	LOSS P TOT 0.036 0.034 0.044 0.062 0.019 0.052 0.033	ARAM PROF 0.038 0.034 0.044 0.062 0.019 0.052 0.053 0.029

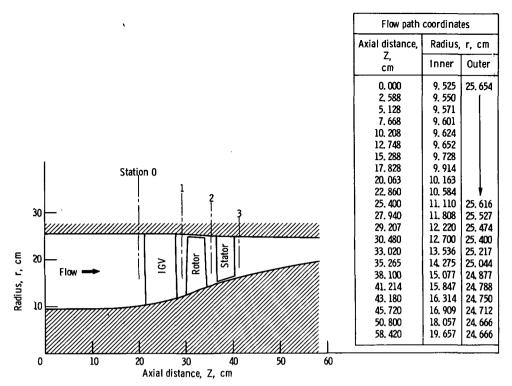


Figure 1. - Flow path for IGV and stage showing axial location of instrumentation.

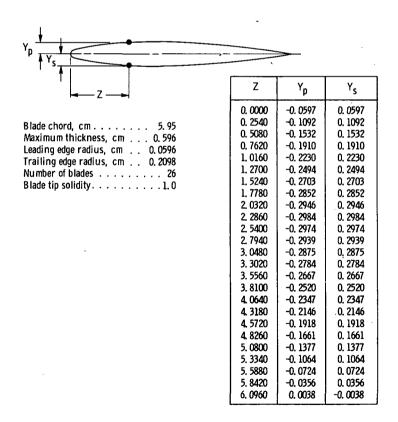
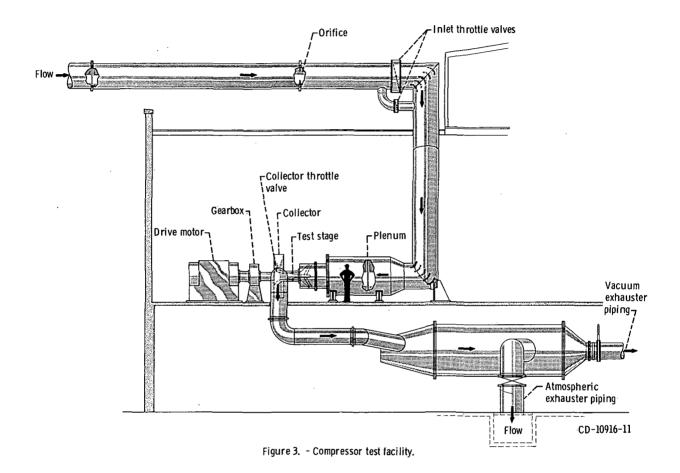
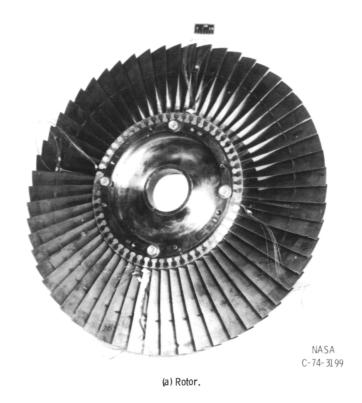


Figure 2. - Inlet guide vane.







(b) Compressor casing with IGV's and stators installed.

Figure 4. - Test hardware.

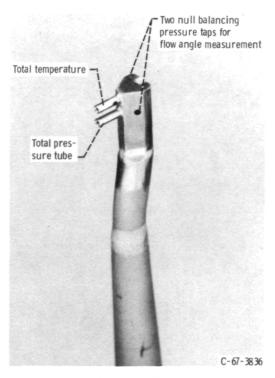


Figure 5. - Combination total pressure, total temperature, and flow angle survey probe (double barrel).

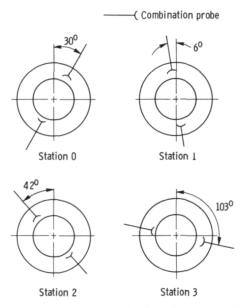


Figure 6. - Circumferential locations of measurements (looking downstream; clockwise rotation).

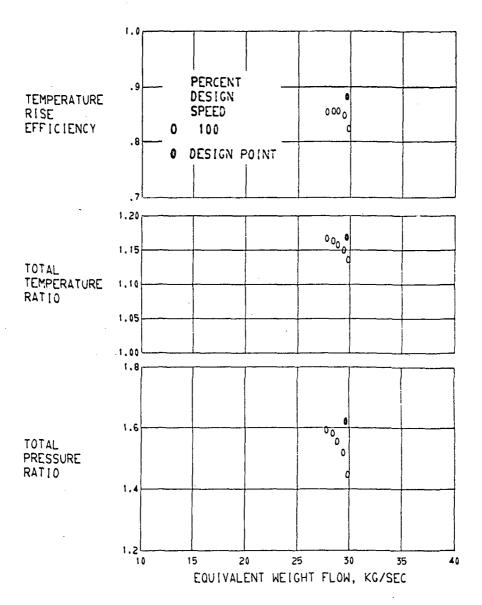


FIGURE 7. - OVERALL PERFORMANCE FOR ROTOR 66.

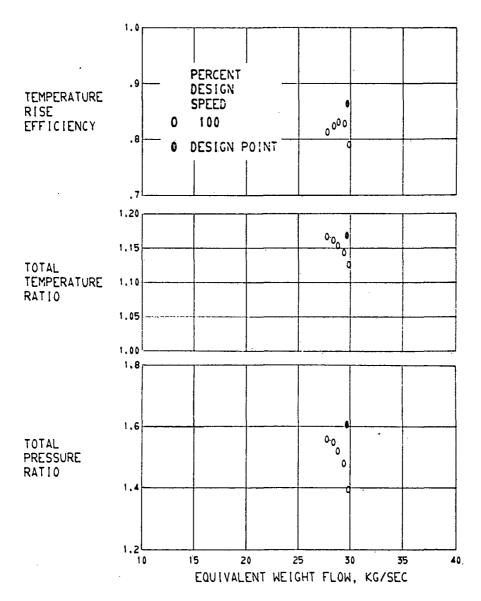


FIGURE 8. - OVERALL PERFORMANCE FOR STAGE 66-66.

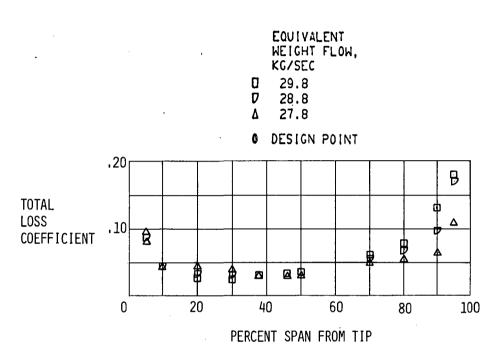
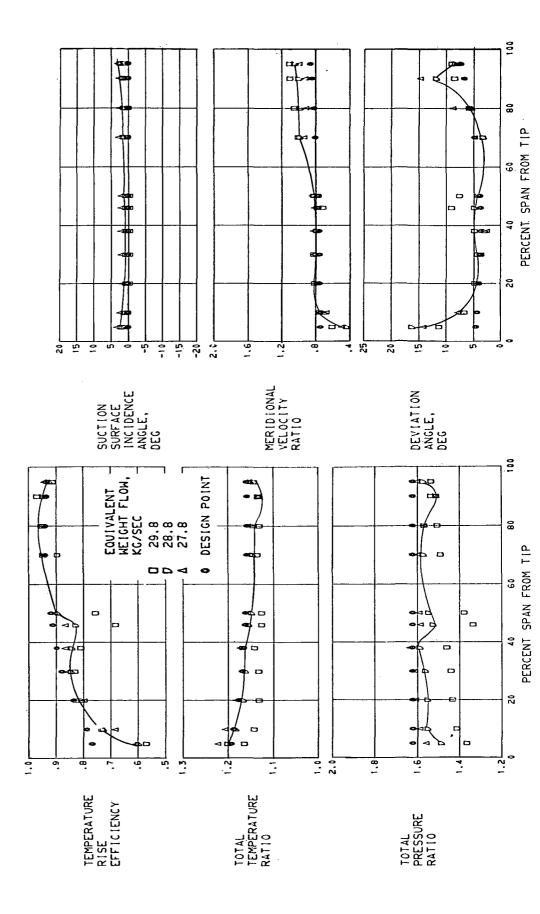


Figure 9. - Radial distribution of inlet guide vane total LOSS COEFFICIENT.



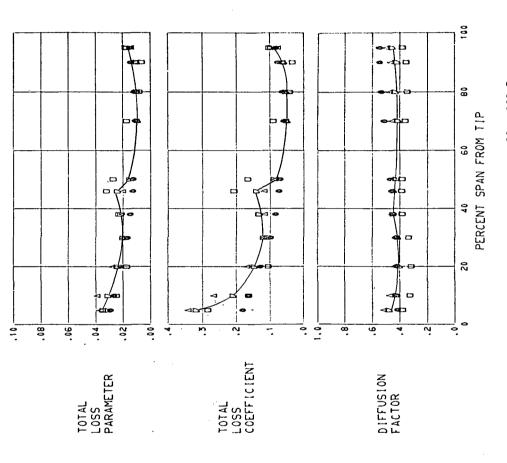


FIGURE 10. - RADIAL DISTRIBUTION OF PERFORMANCE FOR ROTOR 66. 100 PERCENT DESIGN.

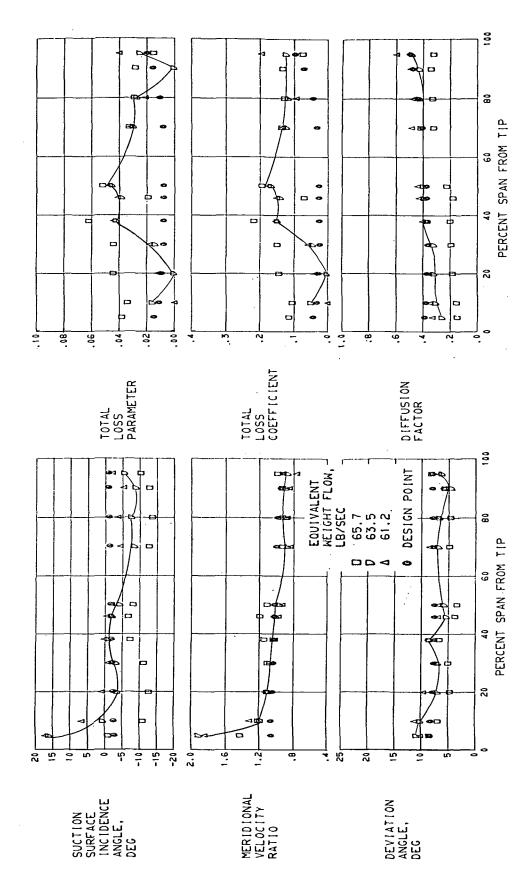
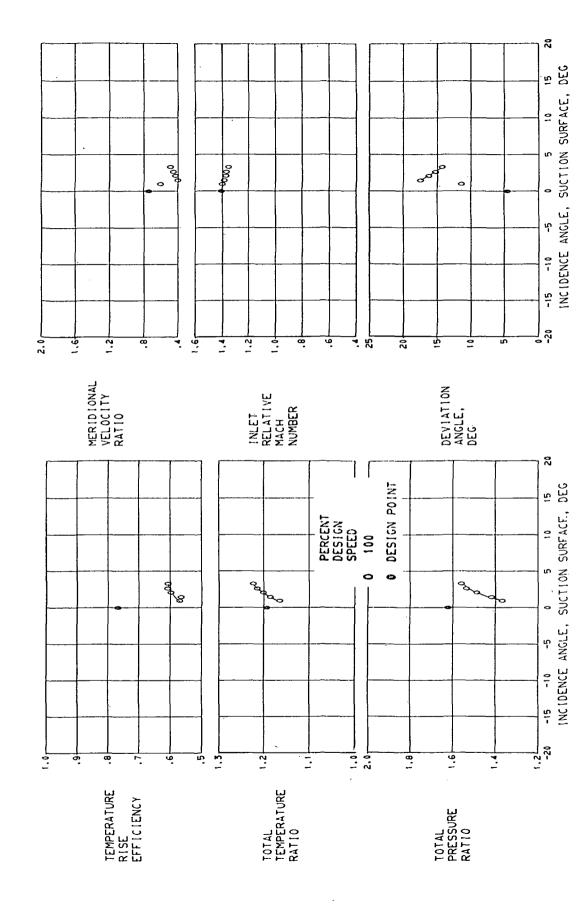


Figure 11. - Radial distribution of Performance for stator 66. 100 Percent design speed.

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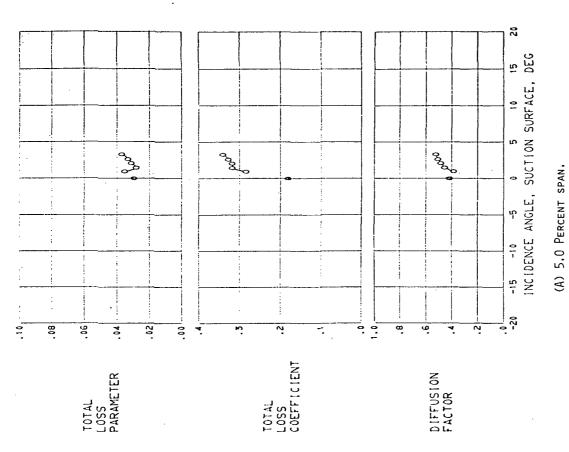
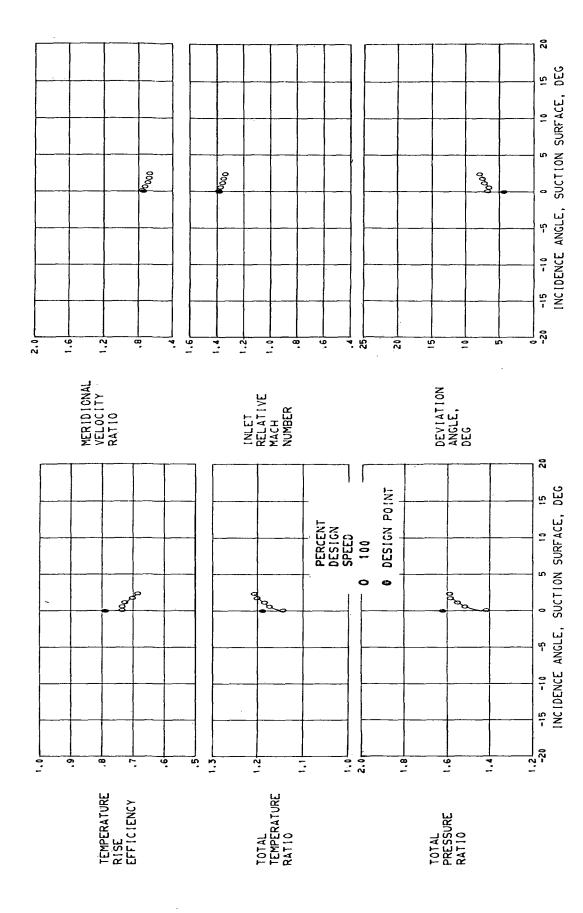


FIGURE 12. - BLADE-ELEMENT PERFORMANCE FOR ROTOR 66.



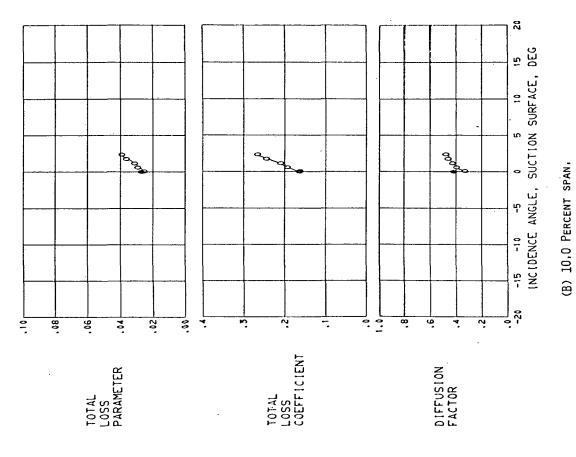
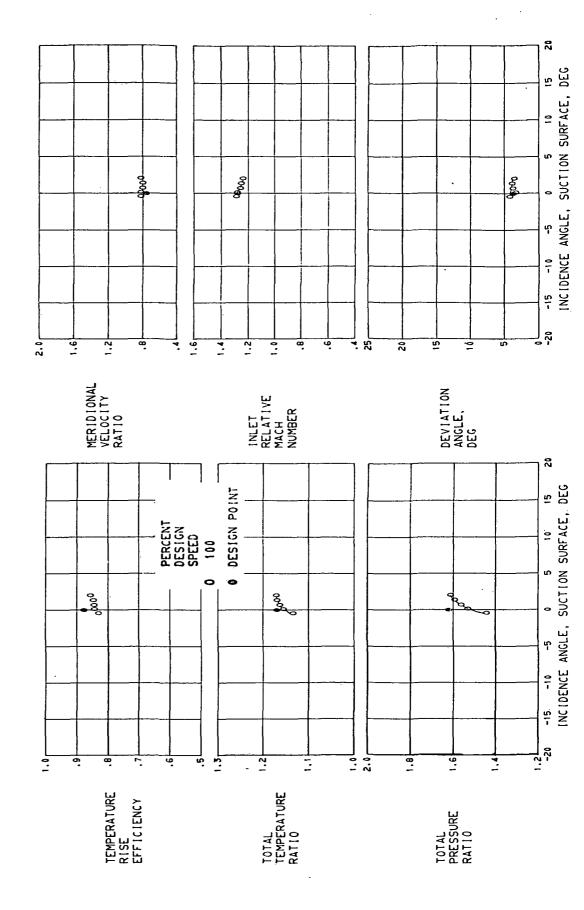


FIGURE 12, - CONTINUED, BLADE-ELEMENT PERFORMANCE FOR ROTOR 66.



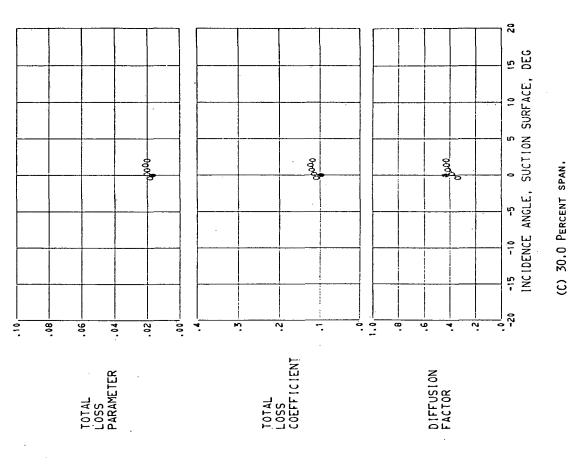
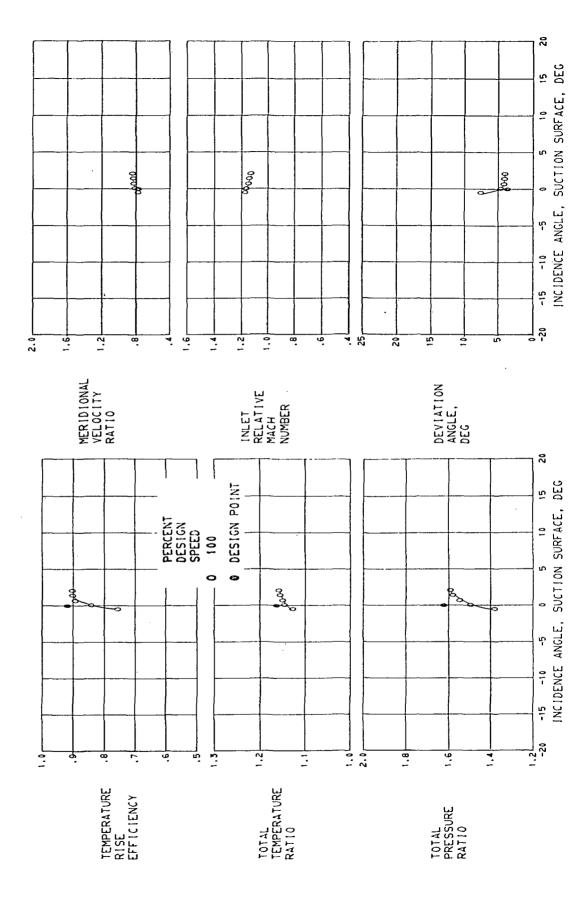


Figure 12, - Continued. Blade-element performance for rotor 66.



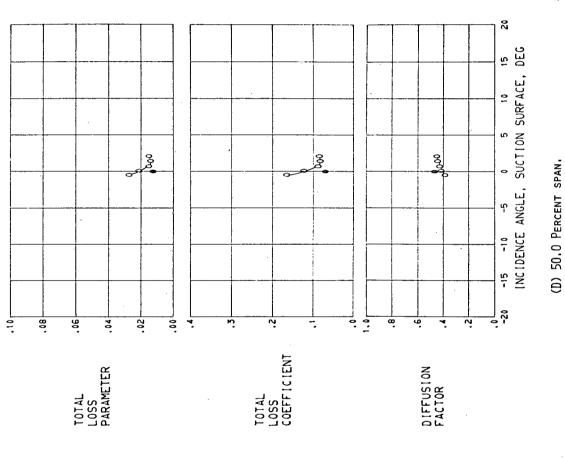
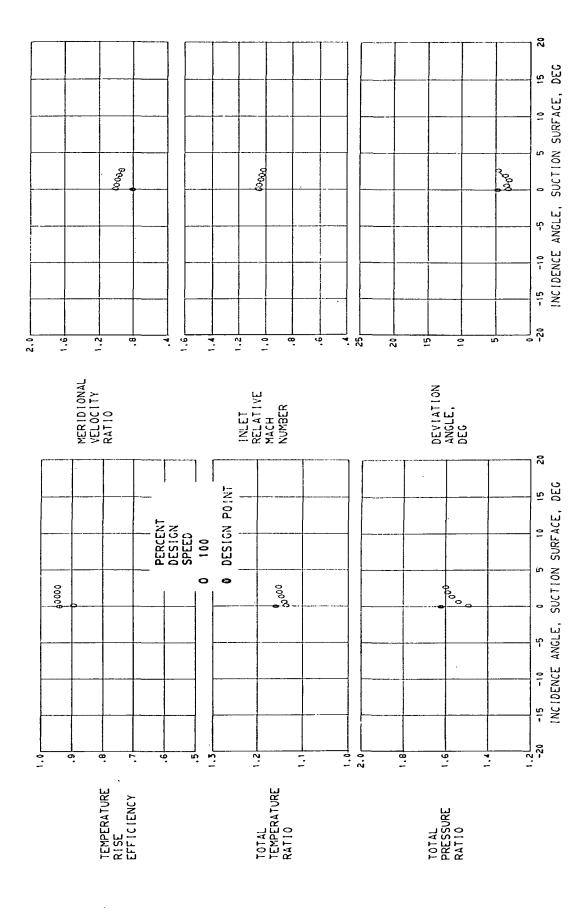


FIGURE 12, - CONTINUED, BLADE-ELEMENT PERFORMANCE FOR ROTOR 66,



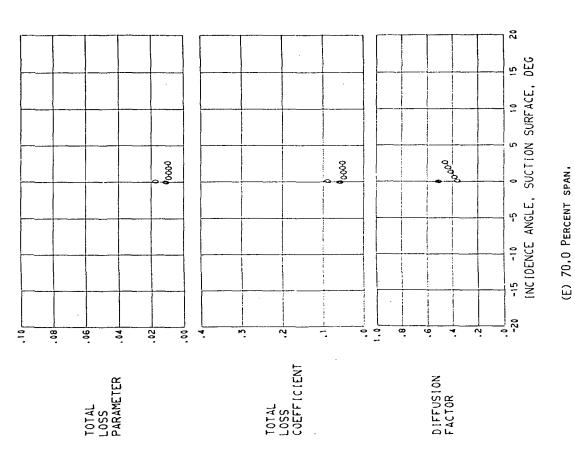
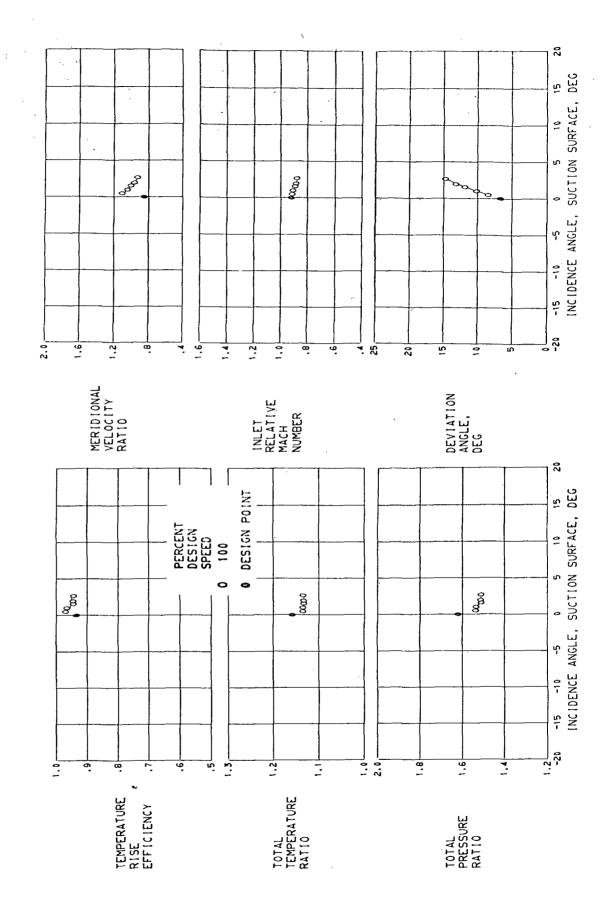


FIGURE 12. - CONTINUED. BLADE-ELEMENT PERFORMANCE FOR ROTOR 66.



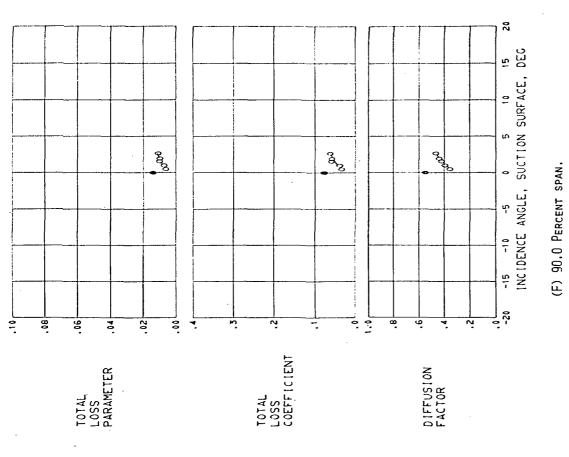
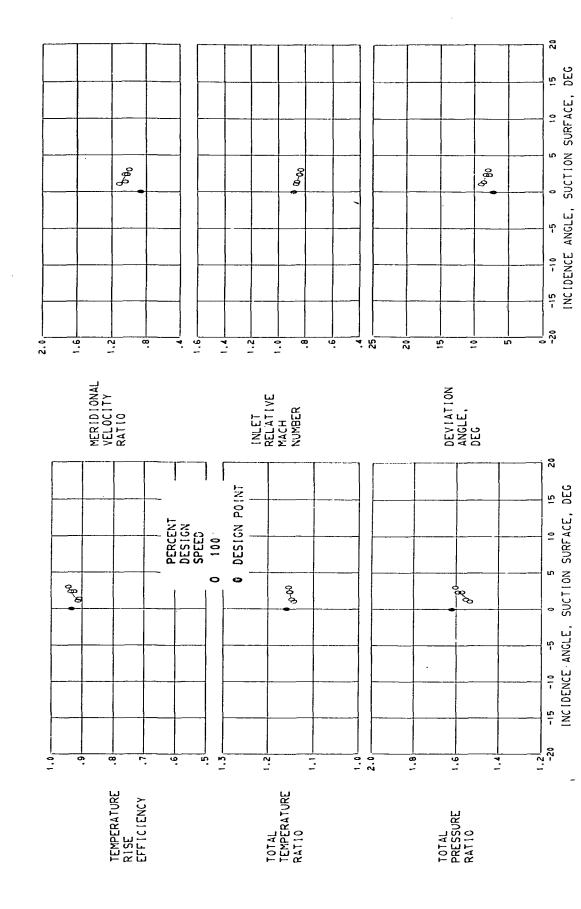


FIGURE 12, - CONTINUED. BLADE-ELEMENT PERFORMANCE FOR ROTOR 66,



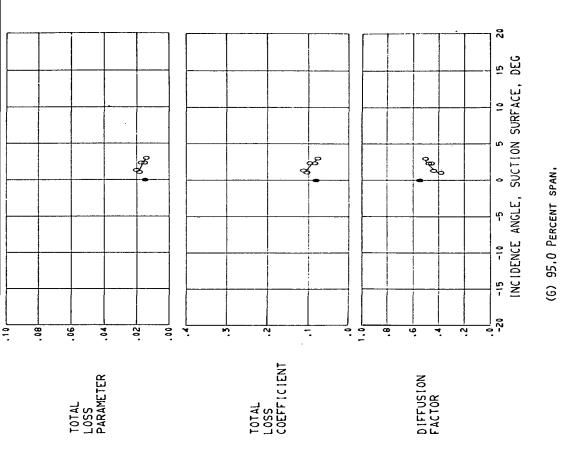


Figure 12. - Concluded. Blade-element performance for rotor 66.

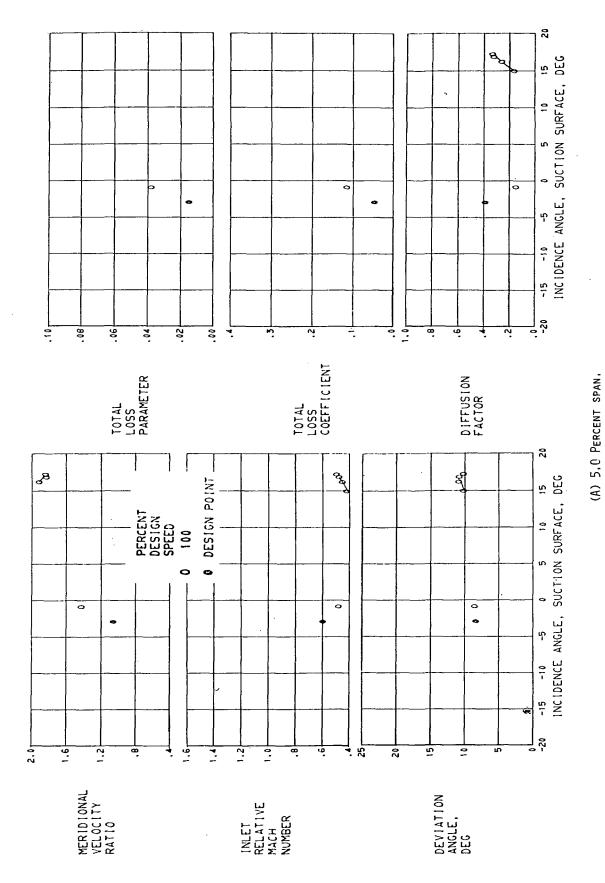


Figure 13. - Blade-element performance for stator 66.

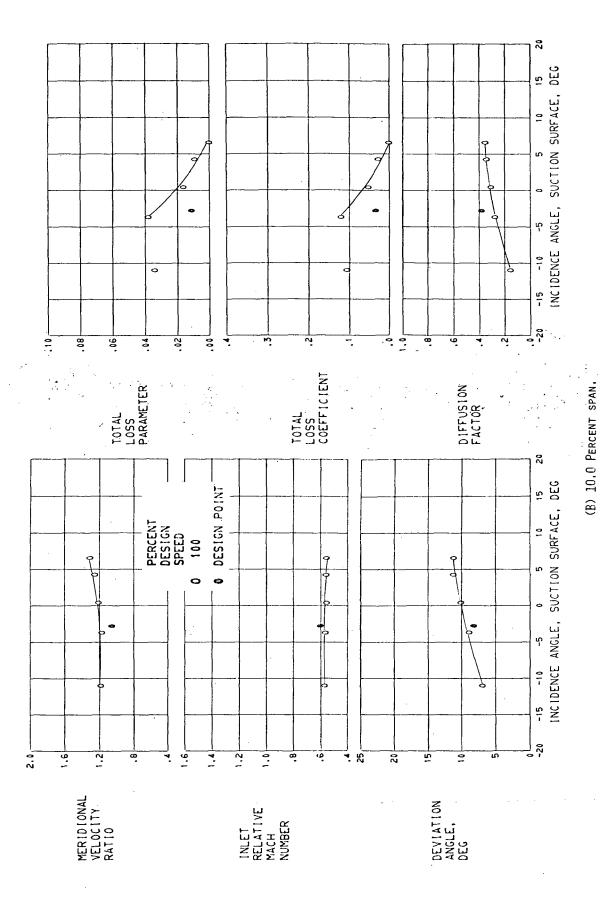


Figure 13. - Continued. Blade-element performance for stator 66.

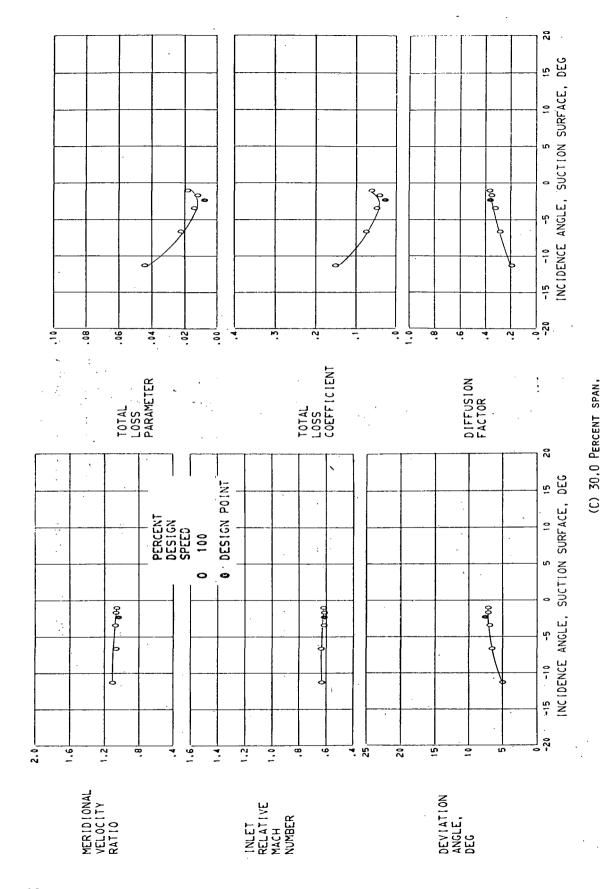


FIGURE 13. - CONTINUED. PLADE-ELEMENT PERFORMANCE FOR STATOR 66.

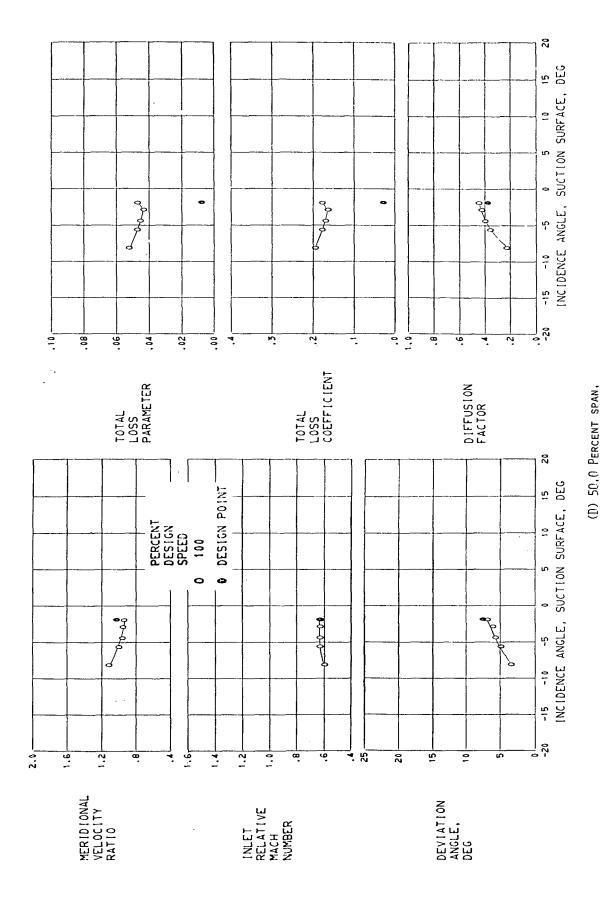


FIGURE 13, - CONTINUED. RLADE-ELEMENT PERFORMANCE FOR STATOR 66.

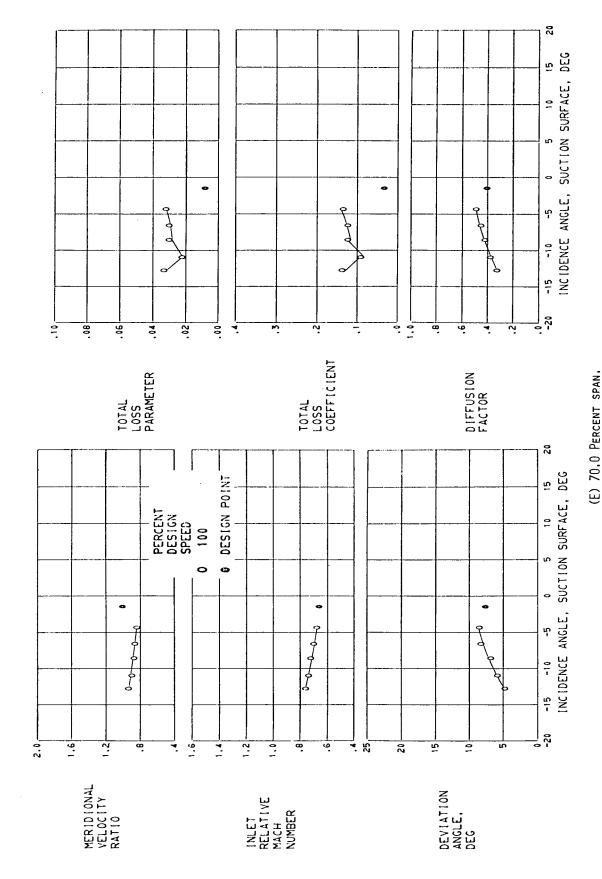


Figure 13. - Continued. Blade-element performance for stator 66.

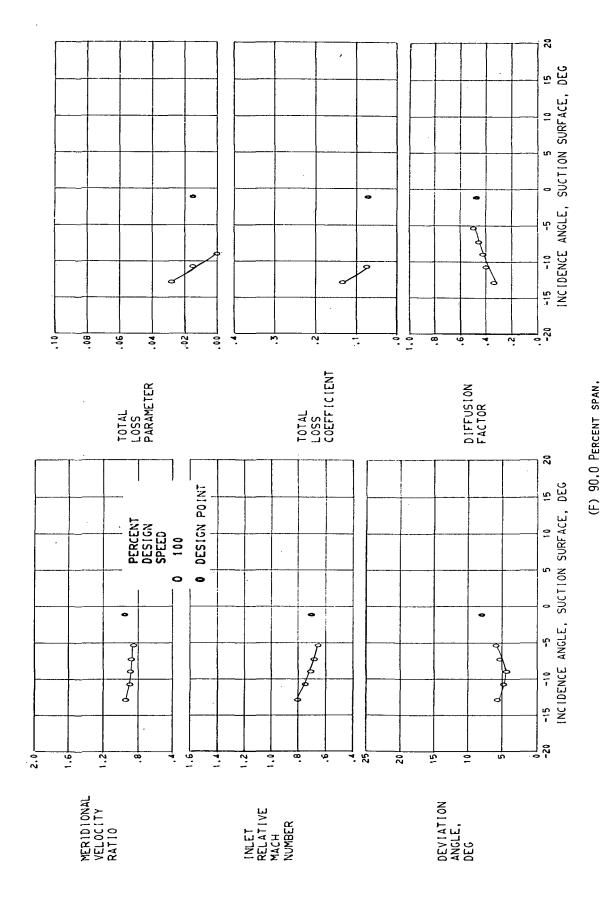


FIGURE 13. - CONTINUED. BLADE-ELEMENT PERFORMANCE FOR STATOR 66.

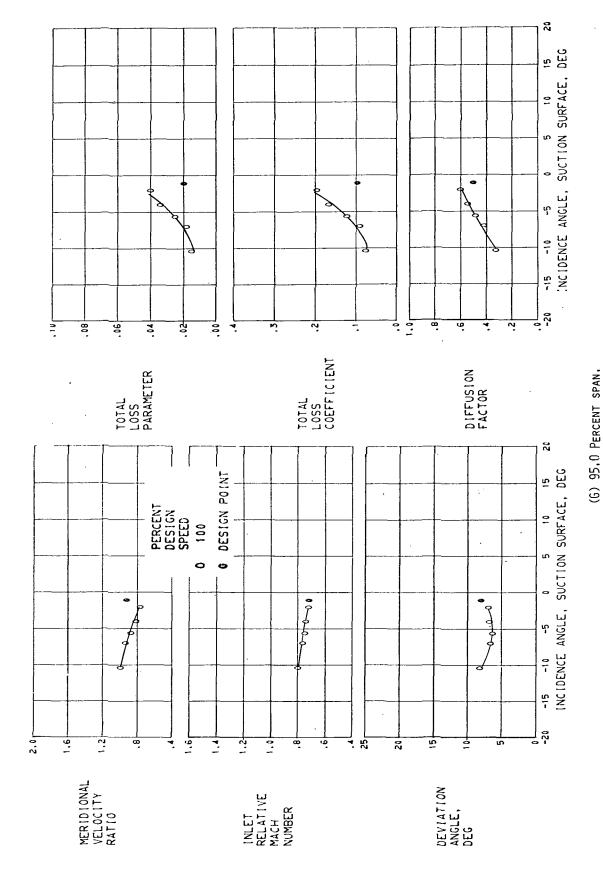


FIGURE 13. - CONCLUDED. BLADE-ELEMENT PERFORMANCE FOR STATOR 66.

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